

AD-A070 595

MARYLAND UNIV COLLEGE PARK DEPT OF PHYSICS AND ASTRONOMY F/G 7/4  
DENSITY SENSITIVE LINES FROM SELECTED MEMBERS OF THE SODIUM-LIK--ETC(U)  
NOV 77 M BLAHA, J DAVIS

N00014-75-C-0309

NL

UNCLASSIFIED

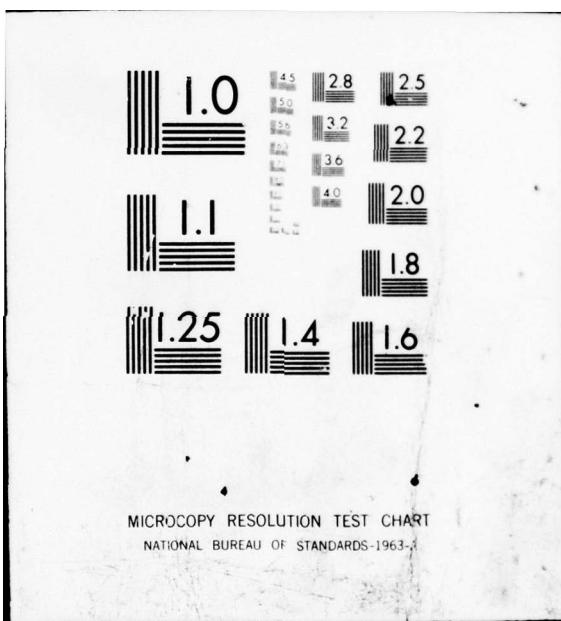
1 OF 1  
AD  
A070595

REF ID:



END  
DATE  
FILED

8-79  
DDC



*6702*

DENSITY SENSITIVE LINES FROM SELECTED MEMBERS  
OF THE SODIUM-LIKE ISOELECTRONIC SEQUENCE

**ADA070595**

J. Davis  
Plasma Dynamic Branch  
Plasma Physics Division

and

M. Blaha  
Department of Physics and Astronomy  
University of Maryland

**APPROVED FOR PUBLIC RELEASE  
DISTRIBUTION UNLIMITED**

November 1977

Work on this report was supported  
by ONR Contract N00014-75-C-0309  
and/or N00014-67-A-0239  
monitored by NRL Code 6702.

79 00 4497

2023

## **DISCLAIMER NOTICE**

**THIS DOCUMENT IS BEST QUALITY  
PRACTICABLE. THE COPY FURNISHED  
TO DDC CONTAINED A SIGNIFICANT  
NUMBER OF PAGES WHICH DO NOT  
REPRODUCE LEGIBLY.**

ADA070595

DDC ACCESSION NUMBER

IV

LEVEL

DDC PROCESSING DATA

PHOTOGRAPH

THIS SHEET

I

INVENTORY

RETURN TO DDA-2 FOR FILE

Density Sensitive Lines from Selected Members----

DOCUMENT IDENTIFICATION

Davis, Blaha

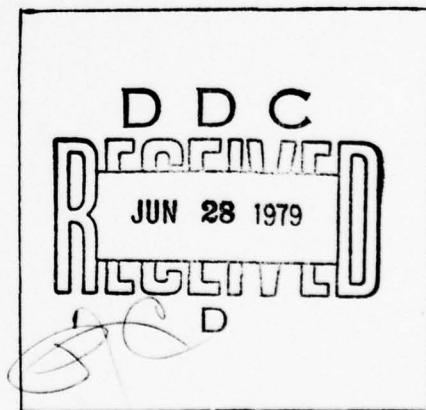
**DISTRIBUTION STATEMENT A**

Approved for public release;  
Distribution Unlimited

DISTRIBUTION STATEMENT

Accession For	
NTIS GRA&I	<input checked="" type="checkbox"/>
DDC TAB	<input type="checkbox"/>
Unannounced	<input type="checkbox"/>
Justification	<input type="checkbox"/>
By _____	
Distribution/	
Availability Codes	
Dist.	Avail and/or special
A	23 RDL

DISTRIBUTION STAMP



DATE ACCESSIONED

79 06 27 297

DATE RECEIVED IN DDC

PHOTOGRAPH THIS SHEET

RETURN TO DDA-2

ABSTRACT

Relative intensities of spectral lines in the sodium isoelectronic sequence are presented. Results are presented for ions of calcium, iron, zinc, krypton and molybdenum for transitions between the  $n = 3$  and  $n = 4$  levels.

79-06-22-97

## I. Introduction

The spectral emission features observed from high temperature plasmas can provide a wealth of information on conditions within the plasma. For plasmas of moderate densities the low lying excited state populations of highly charged ions are governed by electron collision and radiative decay rates. Once the level populations are known it is possible to establish the plasma temperature and density by spectroscopic techniques. One such method is to determine the intensity ratio of selected spectral lines.

In this report calculations have been done for spectral line ratios that exhibit a strong density dependence. Results are presented for the sodium-like ions of calcium, iron, zinc, krypton and molybdenum for transitions between the  $n = 3$  and  $n = 4$  levels.

## II. Results and Discussion

Relative intensities of spectral lines in the sodium isoelectronic sequence presented in this report are derived from the electron-impact collision cross sections and transition probabilities given in a previous paper.<sup>1</sup> In the calculation of relative intensities we have ignored the splitting of all levels in all ions and therefore our results do not represent relative intensities of individual lines but rather the relative intensities of multiplets.

Collision strengths  $\Omega(3s, 3p)$  and  $\Omega(3p, 3d)$  for Zn XX, Kr XXVI and Mo XXXII were obtained from Table 4 of ref. 1 using the relations

$$\Omega(3s, 3p) = \Omega(3s_{1/2}, 3p_{1/2}) + \Omega(3s_{1/2}, 3p_{3/2}),$$

$$\Omega(3p, 3d) = \Omega(3p_{1/2}, 3d) + \Omega(3p_{3/2}, 3d).$$

The corresponding transition probabilities were recalculated from values in Table 3 of ref. 1 for the center of gravity of the 3p term. The effective wavelengths of the multiplets adopted in our calculation are given in Table 1.

Recently Burkhalter et al.<sup>2</sup> identified a number of spectral lines of Mo XXXII. Our extrapolated term values (see ref. 1) agree with observed values within 1% except for the 3d term where the difference is 2.5%. The effect of this change in energy levels on line intensities is practically negligible with the exception of the 4f - 4d transition. The observed energy difference for this multiplet is 21% smaller than our extrapolated value.

A subset of the equations of statistical equilibrium for the population of atomic levels with principal quantum number less than  $n = 5$  were solved with the assumption of an optically thin plasma. The excited level populations were determined by a balance between electron collisional excitation and electron collisional de-excitation and spontaneous radiative decay. All density effects on atomic levels and on collisional cross sections were ignored. In particular, multiple collisions were neglected as were contributions from ionization and recombination processes.

In an optically thin plasma, the intensity of a spectral line corresponding to the transition between levels i and k is given by

$$I_{i \rightarrow k} = (4 \pi)^{-1} N_i \ell A_{ik} E_{ik},$$

where  $N_i$  is the density of atoms excited to the level  $i$ ,  $\ell$  the length of the emitting column,  $A_{ik}$  the coefficient of transition probability and  $E_{ik}$  the energy of the emitted photon.

Relative intensities of multiplets  $nl - n'l'$  with respect to the  $3p - 3s$  transition are shown in Tables 2 - 26 for ten values of the temperature  $T$  ( $kT$  given in eV) and ten electron densities (LOG  $N$  means  $\log N_e$  and  $N_e$  is given in  $\text{cm}^{-3}$ ). The intensity ratios are shown in a semi-logarithmic form (e.g. 7.23-03 means  $7.23 \times 10^{-3}$  etc.).

The dependence of some typical intensity ratios on electron density at one representative temperature for each ion is displayed on Figures 1 - 5.

Using a similar method, Feldman et al.<sup>3</sup> and Feldman and Doschek<sup>4</sup> obtained the ratio  $R = I(3d_{5/2} - 3p_{3/2}) / I(3p_{3/2} - ^3s_{1/2})$  for Fe XVI as a function of electron density. Their results may be compared with our values assuming that the population of individual  $J$  - sublevels of the  $nl$  level is proportional to the statistical weight  $2J + 1$ . We find that our curve representing the ratio  $R$  is shifted to lower values of  $N_e$  as compared to curves in ref. 3 and 4, so that electron densities derived from a given ratio  $R$  are slightly smaller if our results are used. The disagreement is most pronounced around  $N_e = 10^{18}$ , where our curve gives the electron density about two times smaller. The difference is probably caused by higher excitation cross sections used in our calculation.

At electron densities about  $10^{20} \text{ cm}^{-3}$ , the screening effect of free electrons on atomic levels can not be neglected and our results for

relative intensities should be regarded as a limiting case. Also, at such high densities the optical depth of resonance lines may not be negligible even if the emitting region is very small. In this density regime the results presented in Tables 2 - 26 should be applied with caution.

Acknowledgement

This work was supported by the U.S. Energy Research and Development Administration.

References

1. M. Blaha and J. Davis, J. Quant. Spectrosc. Rad. Transfer, in press.
2. P. G. Burkhalter, J. Reader, and R. D. Cowan, J. Opt. Soc. Am., in press.
3. U. Feldman, G. A. Doschek, D. K. Prinz, and D. T. Nagel, J. Appl. Phys. 47, 1341 (1976).
4. U. Feldman and G. A. Doschek, J. Opt. Soc. Am. 67, 726 (1977).

TABLE 1

Adopted effective wavelengths ( $\text{\AA}$ ) of multiplets.

Transition	Ca X	Fe XVI	Zn XX	Kr XXVI	Mo XXXII
3p - 3s	563.06	343.48	267.70	191.46	141.82
3d - 3p	417.08	259.00	205.94	156.67	123.76
4s - 3p	152.62	63.44	41.57	25.19	16.87
4p - 3s	111.04	50.42	34.12	21.26	14.47
4p - 3d	206.95	76.56	48.28	28.23	18.52
4d - 3p	123.49	54.53	36.55	22.62	15.35
4f - 3d	167.00	66.33	42.66	25.49	16.93
4p - 4s	1476.3	862.94	661.74	475.09	354.67
4d - 4p	1151.9	707.06	558.11	416.77	325.33
4f - 4d	3474.7	1664.3	1071.5	711.04	505.23

Ca X

$T = 150 \text{ eV}$

2

$\log_{10}$

$$\frac{I(NL - N'L')}{I(3P - 3S)}$$

1

0

-1

-2

14

16

18

20

22

$\log_{10} N_e$

FIG. 1.

3 Fe XVI

4F - 3D

T = 250 eV

2

$\log_{10}$

$$\frac{I(NL - N'L')}{I(3P - 3S)}$$

1

0

-1

-2

14

16

18

20

22

$\log_{10} N_e$

FIG. 2

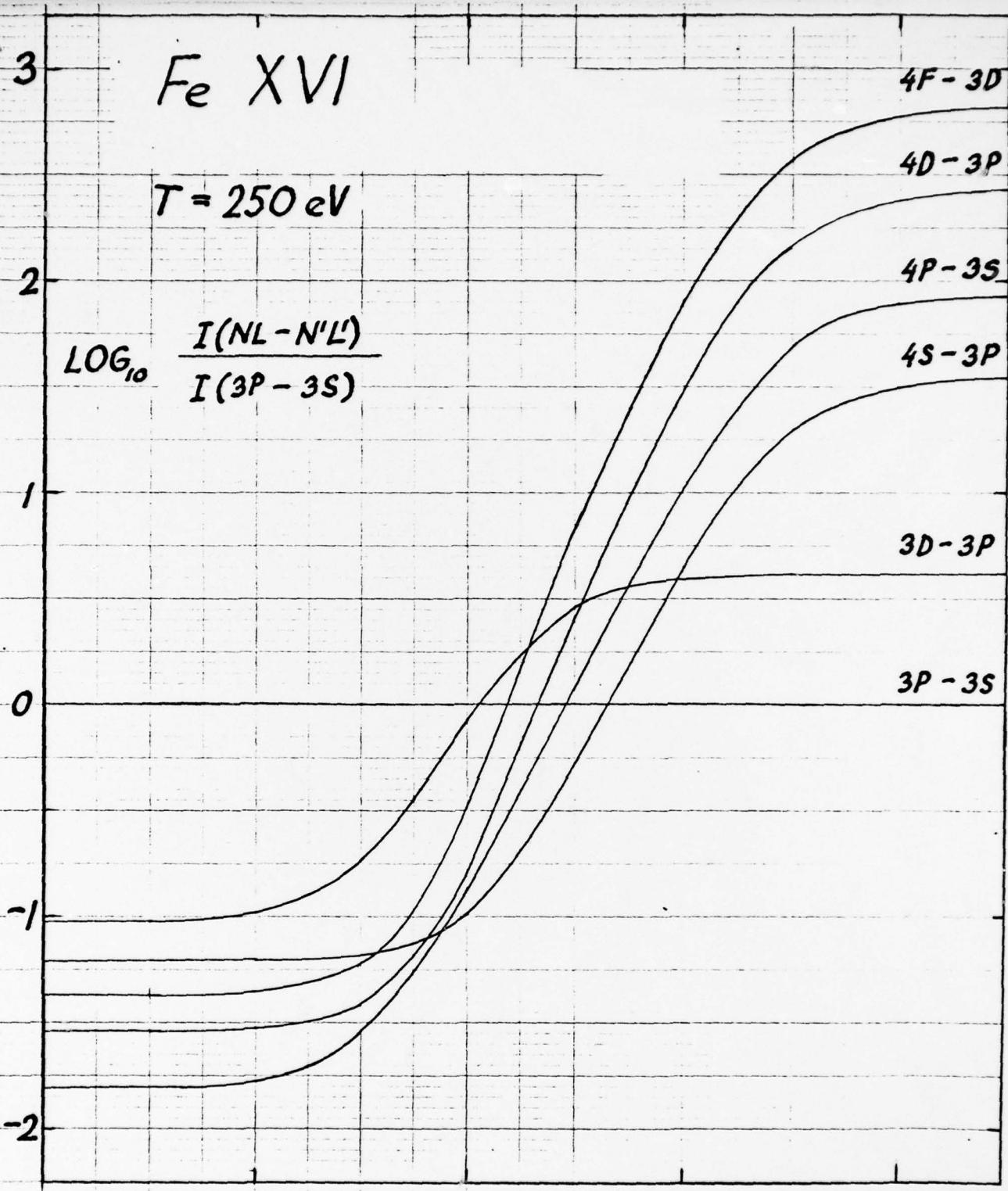
4D - 3P

4P - 3S

4S - 3P

3D - 3P

3P - 3S



Zn XX

$T = 500 \text{ eV}$

3

2

1

0

-1

-2

14

16

18

20

22

$\log_{10}$

$$\frac{I(NL - NL')}{I(3P - 3S)}$$

3D-3P

3P-3S

$\log_{10} N_e$

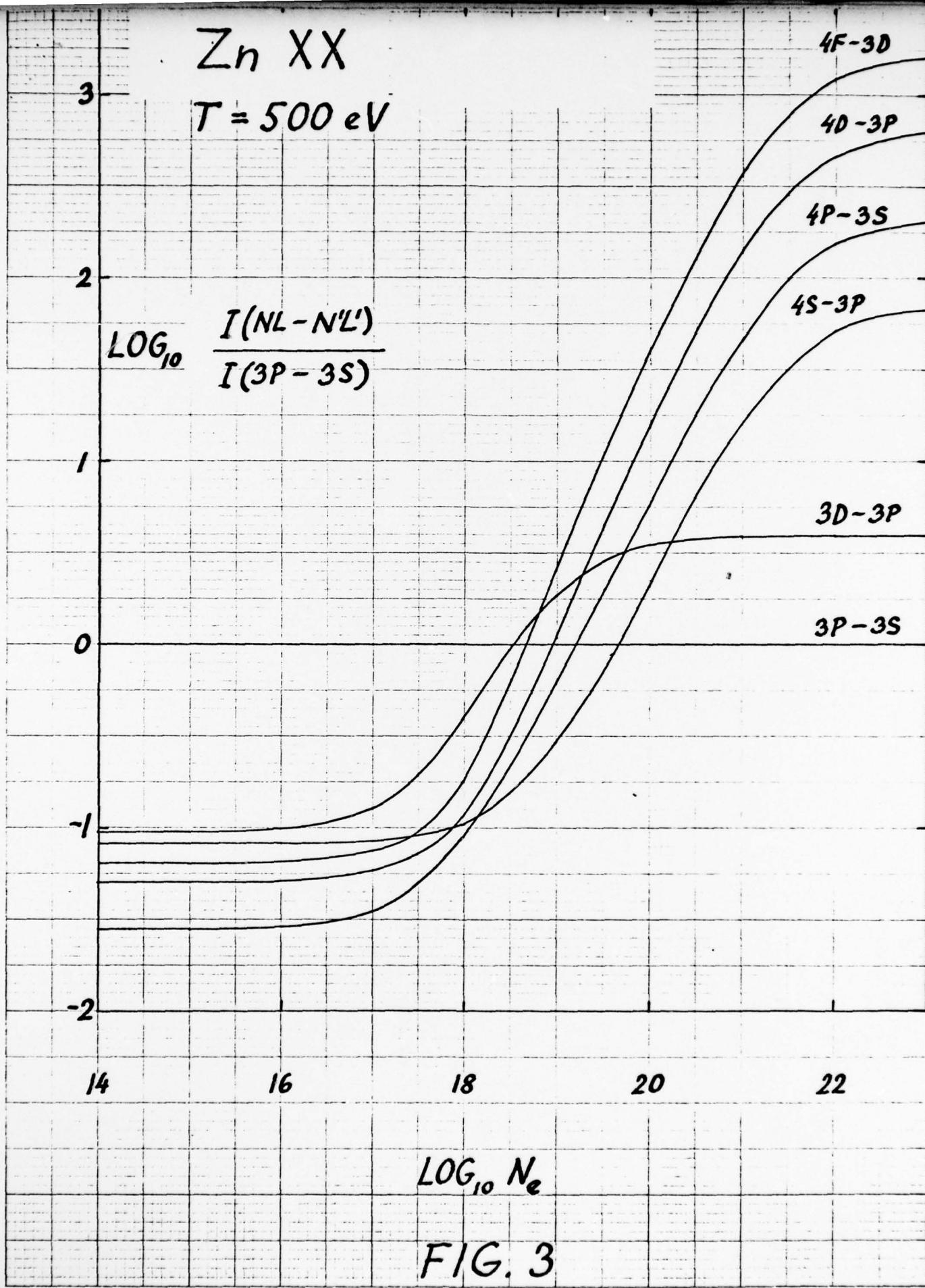
FIG. 3

4F-3D

4D-3P

4P-3S

4S-3P



Kr XXVI

3

$T = 750 \text{ eV}$

2

$$\log_{10} \frac{I(NL - N'L')}{I(3P - 3S)}$$

1

0

-1

16

18

20

22

$\log_{10} N_e$

4F-3D

4D-3P

4P-3S

4S-3P

3D-3P

3P-3S

FIG. 4

Mo XXXII

$T = 1000 \text{ eV}$

$$\log_{10} \frac{I(NL - N'L')}{I(3P - 3S)}$$

3

2

1

0

-1

16

18

20

22

24

$3D - 3P$

$3P - 3S$

$4F - 3D$

$4D - 3P$

$4P - 3S$

$4S - 3P$

$\log_{10} N_e$

FIG. 5

TABLE 2

## CALCIUM X

INTENSITY RATIO  $I(\text{M}^{\text{+}} \text{L} - \text{M}'\text{L}')/I(\text{3P} - \text{3S})$ 

T(EV)	LOG N	3L-3P	4S-3P	4P-3S	4P-3D	4D-3P	4F-3P	4P-4S	4D-4P	4F-4P
10	13	7.23-03	4.10-05	2.32-06	6.92-07	1.50-06	2.60-06	4.48-09	6.24-09	4.35-11
10	14	7.32-03	4.11-05	2.38-06	7.09-07	1.51-06	2.48-06	4.59-09	6.27-09	4.14-11
10	15	8.24-03	4.15-05	2.93-06	8.73-07	1.58-06	2.73-06	5.66-09	6.57-09	4.56-11
10	16	1.72-02	4.54-05	8.38-06	2.50-06	2.52-06	4.38-06	1.62-08	1.05-08	7.32-11
10	17	8.47-02	9.14-05	5.94-05	1.77-05	2.55-05	4.07-05	1.15-07	1.06-07	6.80-10
10	18	2.49-01	6.42-04	5.26-04	1.57-04	4.22-04	8.40-04	1.02-06	1.75-06	1.40-08
10	19	3.14-01	3.62-03	2.94-03	8.77-04	2.62-03	5.69-03	5.68-06	1.09-05	9.50-08
10	20	3.23-01	6.60-03	5.34-03	1.59-03	4.82-03	1.06-02	1.03-05	2.00-05	1.77-07
10	21	3.23-01	7.18-03	5.82-03	1.74-03	5.25-03	1.15-02	1.12-05	2.18-05	1.93-07
10	22	3.23-01	7.25-03	5.87-03	1.75-03	5.30-03	1.16-02	1.13-05	2.20-05	1.94-07
20	13	3.07-02	2.18-03	1.99-04	5.92-05	2.11-04	4.47-04	3.83-07	8.79-07	7.48-09
20	14	3.18-02	2.18-03	2.02-04	6.02-05	2.12-04	4.49-04	3.90-07	8.82-07	7.51-09
20	15	3.39-02	2.19-03	2.35-04	7.00-05	2.20-04	4.66-04	4.53-07	9.13-07	7.79-09
20	16	6.22-02	2.33-03	5.57-04	1.66-04	3.10-04	6.61-04	1.07-06	1.29-06	1.10-08
20	17	2.92-01	4.00-03	3.49-03	1.04-03	2.31-03	4.50-03	6.74-06	9.61-06	7.53-08
20	18	9.93-01	2.52-02	3.07-02	9.16-03	4.09-02	9.70-02	5.93-05	1.70-04	1.62-06
20	19	1.35+00	1.64-01	2.02-01	6.01-02	3.05-01	7.90-01	3.89-04	1.27-03	1.32-05
20	20	1.40+00	3.51-01	4.30-01	1.28-01	6.59-01	1.72+00	8.30-04	2.74-03	2.68-05
20	21	1.40+00	3.95-01	4.84-01	1.44-01	7.43-01	1.95+00	9.35-04	3.09-03	3.25-05
20	22	1.40+00	4.00-01	4.91-01	1.46-01	7.53-01	1.97+00	9.47-04	3.13-03	3.30-05

TABLE 3

## CALCIUM X

INTENSITY RATIO  $I(\text{H}\ \text{L} - \text{H}'\ \text{L}')/I(3\text{P} - 3\text{S})$ 

T(EV)	LNG	H	3D-3P	4S-3P	4P-3S	4P-3D	4P-3F	4F-3L	4P-3S	4F-4IP	4F-4D
50	13	7.26-02	2.21-02	3.00-03	8.96-04	4.07-03	5.97-03	5.80-06	1.69-05	1.50-07	
50	14	7.31-02	2.21-02	3.03-03	9.05-04	4.08-03	4.99-03	5.86-06	1.69-05	1.50-07	
50	15	7.79-02	2.22-02	3.33-03	9.93-04	4.18-03	9.24-03	6.43-06	1.74-05	1.54-07	
50	16	1.25-01	2.31-02	6.26-03	1.87-03	5.35-03	1.20-02	1.21-05	2.22-05	2.00-07	
50	17	5.30-01	3.43-02	3.29-02	9.80-03	2.73-02	5.96-02	6.35-05	1.13-04	9.97-07	
50	18	2.10+00	1.63-01	2.81-01	8.37-02	4.93-01	1.29+00	5.42-04	2.05-03	2.16-05	
50	19	3.17+00	1.38+00	2.17+00	6.49-01	4.51+00	1.30+01	4.20-03	1.88-02	2.17-04	
50	20	3.36+00	3.65+00	5.74+00	1.71+00	1.21+01	3.52+01	1.11-02	5.03-02	5.86-04	
50	21	3.38+00	4.35+00	6.84+00	2.04+00	1.44+01	4.20+01	1.32-02	6.07-02	7.03-04	
50	22	3.39+00	4.43+00	6.98+00	2.08+00	1.47+01	4.29+01	1.35-02	6.12-02	7.17-04	
75	13	8.77-12	3.57-02	5.67-03	1.69-03	7.84-03	1.70-02	1.09-05	3.26-05	2.83-07	
75	14	8.82-02	3.57-02	5.71-03	1.70-03	7.85-03	1.70-02	1.10-05	3.27-05	2.84-07	
75	15	9.33-02	3.59-02	6.15-03	1.83-03	8.03-03	1.74-02	1.19-05	3.34-05	2.91-07	
75	16	1.43-01	3.72-02	1.05-02	3.13-03	9.98-03	2.19-02	2.03-05	4.15-05	3.66-07	
75	17	5.76-01	5.32-02	5.03-02	1.50-02	4.39-02	9.78-02	9.72-05	1.82-04	1.63-06	
75	18	2.40+00	2.64-01	4.23-01	1.26-01	7.80-01	2.19+00	8.17-04	3.24-03	3.51-05	
75	19	3.80+00	2.09+00	3.47+00	1.04+00	7.72+00	2.28+01	6.71-03	3.21-02	3.61-04	
75	20	4.97+00	6.03+00	1.07+01	2.99+00	2.27+01	6.76+01	1.94-02	9.43-02	1.13-03	
75	21	4.11+00	7.40+00	1.23+01	3.67+00	2.79+01	8.39+01	2.37-02	1.16-01	1.39-03	
75	22	4.12+00	7.57+00	1.26+01	3.75+00	2.85+01	8.50+01	2.43-02	1.18-01	1.42-03	

TABLE 4

## CALCIUM X

INTENSITY RATIO  $I(n'L - n'L') / I(3P - 3S)$ 

T(EV)	LOG N	3D-3P	4S-3P	4P-3S	4P-3D	4D-3P	4F-3D	4P-4S	4D-4P	4F-4D
100	13	9.61-02	4.49-02	7.89-03	2.35-03	1.09-02	2.30-02	1.52-05	4.52-05	3.85-07
100	14	9.66-02	4.49-02	7.94-03	2.37-03	1.09-02	2.31-02	1.53-05	4.53-05	3.96-07
100	15	1.02-01	4.50-02	6.45-03	2.52-03	1.11-02	2.36-02	1.63-05	4.63-05	3.94-07
100	16	1.51-01	4.67-02	1.35-02	4.03-03	1.36-02	2.92-02	2.61-05	5.65-05	4.86-07
100	17	5.88-01	6.51-02	6.05-02	1.80-02	5.42-02	1.21-01	1.17-04	2.25-04	2.13-06
100	18	2.53+00	3.08-01	5.03-01	1.50-01	9.45-01	2.58+00	9.72-04	3.93-03	4.31-05
100	19	4.14+00	2.51+00	4.28+00	1.28+00	9.86+00	2.94+01	8.27-03	4.10-02	4.92-04
100	20	4.48+00	7.70+00	1.31+01	3.92+00	3.08+01	9.29+01	2.54-02	1.28-01	1.55-03
100	21	4.53+00	9.64+00	1.65+01	4.91+00	3.87+01	1.17+02	3.18-02	1.61-01	1.95-03
100	22	4.54+00	9.88+00	1.69+01	5.04+00	3.97+01	1.20+02	3.26-02	1.65-01	2.00-03
125	13	1.01-01	5.11-02	9.66-03	2.68-03	1.32-02	2.75-02	1.86-05	5.50-05	4.59-07
125	14	1.02-01	5.11-02	9.71-03	2.90-03	1.33-02	2.75-02	1.88-05	5.51-05	4.60-07
125	15	1.67-01	5.13-02	1.03-02	3.06-03	1.35-02	2.81-02	1.98-05	5.62-05	4.70-07
125	16	1.55-01	5.30-02	1.57-02	4.68-03	1.63-02	3.44-02	3.03-05	6.79-05	5.75-07
125	17	5.88-01	7.29-02	6.64-02	1.98-02	6.06-02	1.36-01	1.28-04	2.52-04	2.27-06
125	18	2.59+00	3.32-01	5.48-01	1.63-01	1.04+00	2.86+00	1.06-03	4.31-03	4.78-05
125	19	4.36+00	2.76+00	4.79+00	1.43+00	1.24+01	3.38+01	9.24-03	4.67-02	5.65-04
125	20	4.74+00	8.86+00	1.54+01	4.59+00	3.69+01	1.12+02	2.97-02	1.53-01	1.67-03
125	21	4.81+00	1.13+01	1.96+01	5.85+00	4.70+01	1.43+02	3.79-02	1.95-01	2.39-03
125	22	4.82+00	1.16+01	2.02+01	6.01+00	4.83+01	1.47+02	3.89-02	2.01-01	2.45-03

TABLE 5

## CALCIUM X

INTENSITY RATIO  $I(\text{H}\alpha)/I(\text{Ly}\alpha) = I(\text{Ly}\beta - \text{Ly}\alpha)$ 

T(°K)	LOG N	3D-3P	4S-3P	4P-3S	4P-3D	4D-3P	4F-3D	4P-4S	4D-4P	4F-4D
150	13	1.05-01	5.55-02	1.11-02	3.30-03	1.51-02	3.18-02	2.14-05	6.27-05	5.15-07
150	14	1.05-01	5.55-02	1.11-02	3.32-03	1.51-02	3.19-02	2.15-05	6.28-05	5.16-07
150	15	1.10-01	5.57-02	1.17-02	3.49-03	1.54-02	3.15-02	2.26-05	6.41-05	5.27-07
150	16	1.57-01	5.75-02	1.73-02	5.16-03	1.84-02	3.32-02	3.34-05	7.66-05	6.38-07
150	17	5.83-01	7.81-02	6.99-02	2.09-02	6.47-02	1.44-01	1.35-04	2.69-14	2.42-16
150	18	2.62+00	3.45-01	5.72-01	1.71-01	1.08+00	3.62+00	1.10-03	4.51-03	5.14-05
150	19	4.50+00	2.91+00	5.10+00	1.52+00	1.21+01	3.68+01	9.86-03	5.65-02	6.14-04
150	20	4.93+00	9.70+00	1.70+01	5.08+00	4.14+01	1.26+02	3.29-02	1.72-01	2.11-03
150	21	5.06+00	1.25+01	2.20+01	6.57+00	5.36+01	1.63+02	4.25+02	2.23+01	2.73+03
150	22	5.01+00	1.29+01	2.27+01	6.76+00	5.52+01	1.68+02	4.38+02	2.29+01	2.61+03
200	13	1.09-01	6.12-02	1.32-02	3.93-03	1.77-02	3.54-02	2.55-05	7.38-05	5.91-07
200	14	1.09-01	6.12-02	1.32-02	3.95-03	1.78-02	3.54-02	2.56-05	7.39-05	5.92-07
200	15	1.14-01	6.14-02	1.38-02	4.12-03	1.81-02	3.61-02	2.67-05	7.52-05	6.13-07
200	16	1.59-01	6.33-02	1.95-02	5.81-03	2.13-02	4.31-02	3.76-05	8.67-05	7.21-07
200	17	5.67-01	8.43-02	7.31-02	2.18-02	6.88-02	1.53-01	1.41-04	2.86-04	2.55-06
200	18	2.62+00	3.54-01	5.90-01	1.76-01	1.11+00	3.14+00	1.14-03	4.63-03	5.25-05
200	19	4.06+00	3.05+00	5.43+00	1.62+00	1.31+01	4.00+01	1.05-02	5.45-02	6.09-04
200	20	5.16+00	1.08+01	1.92+01	5.73+00	4.75+01	1.46+02	3.71-02	1.97-01	2.43-03
200	21	5.25+00	1.43+01	2.54+01	7.58+00	6.29+01	1.93+02	4.91-02	2.62-01	3.23-03
200	22	5.26+00	1.47+01	2.63+01	7.83+00	6.51+01	2.00+02	5.07-02	2.70-01	3.34-03

TABLE 6

## CALCIUM X

INTENSITY RATIOS  $I(\text{L}^{\prime\prime})/I(\text{3P} = 3S)$ 

T(EV)	L	N	3D-3P	4S-3P	4P-3S	4P-3D	4D-3P	4F-3D	4P-4S	4D-4P	4F-4D
250	13	1.11+01	6.46+02	1.47+02	4.37+03	1.96+02	3.33+02	2.83+05	8.13+05	6.40+07	
250	14	1.12+01	6.47+02	1.47+02	4.39+03	1.96+02	3.33+02	2.84+05	8.15+05	6.41+07	
250	15	1.16+01	6.48+02	1.53+02	4.56+03	1.99+02	3.90+02	2.95+05	8.28+05	6.52+07	
250	16	1.59+01	6.68+02	2.08+02	6.21+03	2.32+02	4.61+02	4.02+05	9.67+05	7.71+07	
250	17	5.50+01	8.76+02	7.37+02	2.20+02	7.03+02	1.55+01	1.42+04	2.92+04	2.59+06	
250	18	2.59+00	3.53+01	5.88+01	1.75+01	1.10+00	3.14+00	1.13+03	4.58+03	5.24+05	
250	19	4.75+00	3.08+00	5.53+00	1.65+00	1.35+01	4.14+01	1.07+02	5.61+02	6.92+04	
250	20	5.30+00	1.14+01	2.05+01	6.12+00	5.12+01	1.58+02	3.96+02	2.13+01	2.64+03	
250	21	5.40+00	1.54+01	2.77+01	8.26+00	6.93+01	2.13+02	5.35+02	2.88+01	3.57+03	
250	22	5.41+00	1.60+01	2.87+01	8.56+00	7.18+01	2.21+02	5.54+02	2.99+01	3.77+03	
300	13	1.13+01	6.69+02	1.57+02	4.69+03	2.09+02	4.03+02	3.04+05	8.67+05	6.73+07	
300	14	1.13+01	6.69+02	1.58+02	4.71+03	2.09+02	4.04+02	3.05+05	8.69+05	6.74+07	
300	15	1.17+01	6.71+02	1.63+02	4.87+03	2.12+02	4.10+02	3.15+05	8.82+05	6.86+07	
300	16	1.58+01	6.90+02	2.17+02	6.47+03	2.46+02	4.80+02	4.19+05	1.02+14	8.13+07	
300	17	5.34+01	8.94+02	7.34+02	2.19+02	7.05+02	1.54+01	1.42+04	2.93+04	2.58+06	
300	18	2.55+00	3.47+01	5.78+01	1.72+01	1.07+00	3.08+00	1.12+03	4.46+03	5.14+05	
300	19	4.80+00	3.06+00	5.53+00	1.65+00	1.36+01	4.18+01	1.07+02	5.64+02	6.99+04	
300	20	5.39+00	1.18+01	2.13+01	6.36+00	5.36+01	1.66+02	4.12+02	2.23+01	2.77+03	
300	21	5.51+00	1.62+01	2.93+01	8.74+00	7.38+01	2.28+02	5.66+02	3.07+01	3.61+03	
300	22	5.52+00	1.68+01	3.04+01	9.08+00	7.67+02	2.37+02	5.88+02	3.19+01	3.96+03	

TABLE 7

IRON XVI

INTENSITY RATIO  $I(L_i L_j - 'L_i'L_j)/I(3P - 3S)$ 

T(EV)	LOG N	3D-3P	4S-3P	4F-3S	4F-3D	4D-3P	4F-3D	4P-4S	4D-4P	4F-4D
50	14	4.57-02	3.31-03	4.36-04	1.06-04	8.25-04	1.24-03	2.04-07	5.33-07	9.36-09
50	15	4.04-02	3.32-03	4.45-04	1.08-04	8.29-04	1.25-03	2.08-07	5.35-07	9.42-09
50	16	5.35-02	3.35-03	5.32-04	1.20-04	8.70-04	1.37-03	2.49-07	5.62-07	9.90-09
50	17	1.21-01	3.69-03	1.40-03	3.40-04	1.33-03	2.14-03	6.54-07	8.62-07	1.62-09
50	18	6.04-01	7.46-03	9.84-03	2.39-03	9.88-03	1.93-02	4.60-06	6.38-06	1.46-07
50	19	1.58+00	4.78-02	8.91-02	2.17-02	1.63-01	3.61-01	4.17-05	1.05-04	2.73-06
50	20	1.90+00	3.54-01	6.87-01	1.67-01	1.47+00	3.43+00	3.21-04	6.50-04	2.50-05
50	21	1.94+00	1.16+00	2.27+00	5.52-01	4.96+00	1.17+01	1.06-03	3.21-03	6.15-05
50	22	1.95+00	1.52+00	2.96+00	7.19-01	6.49+00	1.53+01	1.38-03	4.19-03	1.16-04
50	23	1.95+00	1.56+00	3.05+00	7.42-01	6.69+00	1.58+01	1.43-03	4.32-03	1.19-04
75	14	6.17-02	1.16-02	1.81-03	4.41-04	3.65-03	5.62-03	8.48-07	2.35-06	4.24-08
75	15	6.25-02	1.16-02	1.84-03	4.48-04	3.66-03	5.65-03	8.61-07	2.36-06	4.26-08
75	16	7.66-02	1.17-02	2.13-03	5.17-04	3.82-03	5.92-03	9.94-07	2.47-06	4.47-08
75	17	1.49-01	1.27-02	4.96-03	1.21-03	5.54-03	9.66-03	2.72-06	3.58-06	6.84-08
75	18	7.35-01	2.36-02	3.25-02	7.90-03	3.54-02	7.17-02	1.52-05	2.29-05	5.41-07
75	19	2.08+00	1.44-01	2.92-01	7.10-02	5.92-01	1.38+00	1.37-04	3.82-04	1.04-05
75	20	2.59+00	1.16+00	2.35+00	5.70-01	5.63+00	1.38+01	1.10-03	3.64-03	1.04-04
75	21	2.66+00	4.06+00	8.57+00	2.68+00	2.10+01	5.21+01	4.01-03	1.36-02	3.94-04
75	22	2.67+00	5.45+00	1.17+01	2.84+00	2.88+01	7.14+01	5.47-03	1.86-02	5.39-04
75	23	2.67+00	5.66+00	1.21+01	2.95+00	2.99+01	7.47+01	5.68-03	1.93-02	5.61-04

TABLE 9

## IRON XVI

INTENSITY RATIO  $I(\text{H}\alpha) / I(\text{Ly}\alpha - \text{Ly}\beta)$ 

T(KEV)	LOG N	3D-3P	4S-3P	4P-3S	4P-3D	4D-3P	4P-4S	4L-4D	4F-4I
100	14	7.17-02	2.13-02	3.77-03	9.17-04	7.66-03	1.18-02	1.76-06	4.91-06
100	15	7.26-02	2.14-02	3.82-03	9.29-04	7.69-03	1.19-02	1.79-06	4.96-06
100	16	8.11-02	2.15-02	4.32-03	1.05-03	7.98-03	1.24-02	2.02-06	5.15-06
100	17	1.63-01	2.32-02	9.24-03	2.24-03	1.12-02	1.83-02	4.32-06	7.25-06
100	18	7.93-01	4.12-02	5.72-02	1.39-02	6.49-02	1.33-01	2.67-05	4.19-05
100	19	2.37+00	2.41-01	5.11-01	1.24-01	1.08+00	2.60+00	2.39-04	6.98-04
100	20	3.62+00	1.80+00	4.21+00	1.02+00	1.07+01	2.69+01	1.97-03	6.91-03
100	21	3.11+00	7.31+00	1.64+01	3.99+00	4.27+01	1.98+02	7.68-03	2.76-02
100	22	3.12+00	1.63+01	2.32+01	5.64+00	6.05+01	1.54+02	1.98-02	3.91-02
100	23	3.13+00	1.08+01	2.42+01	5.88+00	6.31+01	1.61+02	1.13-02	4.07-02
150	14	8.35-02	3.87-02	8.09-03	1.97-03	1.60-02	2.44-02	3.78-06	1.64-05
150	15	8.44-02	3.87-02	8.17-03	1.99-03	1.61-02	2.45-02	3.82-06	1.64-05
150	16	7.29-02	3.90-02	8.99-03	2.18-03	1.67-02	2.55-02	4.20-06	1.56-05
150	17	1.76-01	4.16-02	1.71-02	4.15-03	2.26-02	3.60-02	7.98-06	1.46-05
150	18	6.32-01	7.02-02	9.63-02	2.34-02	1.14-01	2.33-01	4.50-05	7.38-05
150	19	2.66+00	3.89-01	8.54-01	2.07-01	1.87+00	4.65+00	3.99-04	1.21-03
150	20	3.51+00	3.11+00	7.26+00	1.76+00	1.95+01	5.14+01	3.40-03	1.26-02
150	21	3.64+00	1.31+01	3.09+01	7.51+00	8.51+01	2.22+02	1.44-02	5.49-02
150	22	3.66+00	1.95+01	4.59+01	1.11+01	1.27+02	3.30+02	2.15-02	8.18-02
150	23	3.66+00	2.05+01	4.83+01	1.17+01	1.33+02	3.47+02	2.26-02	8.66-02

TABLE 9

## IRON XVI

INTENSITY RATIO  $I(1s, L - 1s, L')/I(3P - 3S)$ 

T(EV)	LOG N	3D-3P	4S-3P	4P-3S	4P-3D	4D-3P	4F-3S	4F-4S	4D-4P	4F-4P
200	14	9.00-02	5.15-02	1.21-02	2.93-03	2.32-02	3.47-02	5.64-06	1.50-05	2.02-07
200	15	9.09-02	5.15-02	1.22-02	2.96-03	2.33-02	3.48-02	5.69-06	1.51-05	2.03-07
200	16	9.92-02	5.19-02	1.32-02	3.20-03	2.40-02	3.64-02	6.16-06	1.55-05	2.72-07
200	17	1.80-01	5.51-02	2.31-02	5.62-03	3.10-02	4.97-02	1.08-05	2.04-05	3.75-07
200	18	8.31-01	9.00-02	1.21-01	2.95-02	1.48-01	2.98-01	5.67-05	0.54-05	2.25-06
200	19	2.80+00	4.79-01	1.07+00	2.60-01	2.37+00	6.01+00	4.09-04	1.53-03	0.53-05
200	20	3.77+00	3.88+00	9.28+00	2.25+00	2.56+01	6.72+01	4.34-03	1.65-02	5.07-04
200	21	3.93+00	1.73+01	4.18+01	1.02+01	1.18+02	3.12+02	1.95-02	7.65-02	2.36-03
200	22	3.96+00	2.67+01	6.44+01	1.56+01	1.83+02	4.83+02	3.01-02	1.16-01	3.65-03
200	23	3.96+00	2.82+01	6.81+01	1.65+01	1.94+02	5.11+02	3.18-02	1.25-01	3.86-03

TABLE I<sup>a</sup>

## IRON XVI

INTENSITY RATIO  $I(nL + n'L')/I(3P - 3S)$ 

T(EV)	LOG N	3D-3P	4S-3P	4P-3S	4P-3D	4D-3P	4F-3L	4P-4S	4C-3P	4F-4L
300	14	9.67-02	6.76-02	1.84-02	4.46-03	3.36-02	4.66-02	8.58-06	2.17-05	3.07-07
300	15	9.75-02	6.76-02	1.85-02	4.49-03	3.37-02	4.84-02	8.63-06	2.18-05	3.08-07
300	16	1.35-01	6.80-02	1.96-02	4.77-03	3.47-02	5.03-02	9.18-06	2.24-05	3.14-07
300	17	1.81-01	7.19-02	3.13-02	7.59-03	4.48-02	6.71-02	1.46-05	2.89-05	5.06-07
300	18	8.10-01	1.13-01	1.46-01	3.56-02	1.85-01	3.64-01	6.85-05	1.19-04	2.75-05
300	19	2.89-00	5.68-01	1.28-00	3.11-01	2.85-00	7.42-03	5.97-04	1.64-03	5.01-05
300	20	4.04-00	4.67-00	1.14-01	2.77-00	3.22-01	8.63-01	5.33-03	2.08-02	6.51-04
300	21	4.24-00	2.24-01	5.54-01	1.35-01	1.62-02	4.32-02	2.59-02	1.04-01	3.26-03
300	22	4.28-00	3.64-01	9.01-01	2.19-01	2.63-02	7.14-02	4.21-02	1.70-01	5.31-03
300	23	4.28-00	3.80-01	6.61-01	2.33-01	2.81-02	7.51-02	4.49-02	1.81-01	5.67-03
350	14	9.86-02	7.28-02	2.08-02	5.05-03	3.74-02	5.33-02	9.71-06	2.41-05	4.03-07
350	15	9.94-02	7.28-02	2.09-02	5.08-03	3.75-02	5.35-02	9.76-06	2.42-05	4.04-07
350	16	1.07-01	7.32-02	2.21-02	5.36-03	3.85-02	5.51-02	1.03-05	2.49-05	4.16-07
350	17	1.81-01	7.72-02	3.40-02	8.26-03	4.92-02	7.26-02	1.59-05	3.18-05	5.48-07
350	18	7.95-01	1.19-01	1.53-01	3.71-02	1.94-01	3.79-01	7.13-05	1.26-04	2.96-06
350	19	2.90-00	5.84-01	1.32-00	3.22-01	2.95-00	7.76-00	6.19-04	1.91-03	5.95-05
350	20	4.11-00	4.86-01	1.19-01	2.90-00	3.40-01	9.16-01	5.58-03	2.20-02	6.92-04
350	21	4.33-00	2.40-01	5.97-01	1.45-01	1.75-02	4.71-02	2.79-02	1.13-01	3.55-03
350	22	4.37-00	3.98-01	9.90-01	2.41-01	2.92-02	7.83-02	4.63-02	1.89-01	5.01-03
350	23	4.38-00	4.26-01	1.06-02	2.58-01	3.13-02	8.39-02	4.96-02	2.02-01	6.33-03

TABLE II

IRON XVI

INTENSITY RATIO  $I(H_L - H_L') / I(3S - 3S')$ 

$\tau(\text{EV})$	$L\alpha$	$3L - 3P$	$4S - 3P$	$4P - 3S$	$4F - 3D$	$4L - 3P$	$4F - 3D$	$4P - 4S$	$4L - 3P$	$4F - 4D$
400	14	$1 \cdot 09 \pm 0.1$	$7 \cdot 09 \pm 0.2$	$2 \cdot 28 \pm 0.2$	$5 \cdot 54 \pm 0.3$	$4 \cdot 05 \pm 0.2$	$5 \cdot 71 \pm 0.2$	$1 \cdot 07 \pm 0.5$	$2 \cdot 01 \pm 0.5$	$4 \cdot 31 \pm 0.7$
400	15	$1 \cdot 01 \pm 0.1$	$7 \cdot 69 \pm 0.2$	$2 \cdot 29 \pm 0.2$	$5 \cdot 57 \pm 0.3$	$4 \cdot 06 \pm 0.2$	$5 \cdot 73 \pm 0.2$	$1 \cdot 07 \pm 0.5$	$2 \cdot 02 \pm 0.5$	$4 \cdot 32 \pm 0.7$
400	16	$1 \cdot 08 \pm 0.1$	$7 \cdot 73 \pm 0.2$	$2 \cdot 41 \pm 0.2$	$5 \cdot 87 \pm 0.3$	$4 \cdot 16 \pm 0.2$	$5 \cdot 80 \pm 0.2$	$1 \cdot 13 \pm 0.5$	$2 \cdot 02 \pm 0.5$	$4 \cdot 45 \pm 0.7$
400	17	$1 \cdot 79 \pm 0.1$	$8 \cdot 14 \pm 0.2$	$3 \cdot 62 \pm 0.2$	$8 \cdot 79 \pm 0.3$	$5 \cdot 27 \pm 0.2$	$7 \cdot 69 \pm 0.2$	$1 \cdot 69 \pm 0.5$	$3 \cdot 41 \pm 0.5$	$5 \cdot 81 \pm 0.7$
400	18	$7 \cdot 79 \pm 0.1$	$1 \cdot 24 \pm 0.1$	$1 \cdot 56 \pm 0.1$	$3 \cdot 89 \pm 0.2$	$2 \cdot 01 \pm 0.1$	$3 \cdot 88 \pm 0.1$	$7 \cdot 31 \pm 0.5$	$1 \cdot 31 \pm 0.4$	$2 \cdot 93 \pm 0.6$
400	19	$2 \cdot 99 \pm 0.0$	$5 \cdot 99 \pm 0.1$	$1 \cdot 35 \pm 0.0$	$3 \cdot 28 \pm 0.1$	$3 \cdot 00 \pm 0.0$	$7 \cdot 96 \pm 0.0$	$6 \cdot 31 \pm 0.4$	$1 \cdot 64 \pm 0.3$	$6 \cdot 01 \pm 0.5$
400	20	$4 \cdot 17 \pm 0.0$	$4 \cdot 97 \pm 0.0$	$1 \cdot 23 \pm 0.1$	$2 \cdot 99 \pm 0.0$	$3 \cdot 52 \pm 0.1$	$9 \cdot 53 \pm 0.1$	$5 \cdot 74 \pm 0.3$	$2 \cdot 27 \pm 0.2$	$7 \cdot 19 \pm 0.4$
400	21	$4 \cdot 39 \pm 0.0$	$2 \cdot 52 \pm 0.1$	$6 \cdot 29 \pm 0.1$	$1 \cdot 53 \pm 0.1$	$1 \cdot 86 \pm 0.2$	$5 \cdot 00 \pm 0.2$	$2 \cdot 94 \pm 0.2$	$1 \cdot 29 \pm 0.1$	$3 \cdot 78 \pm 0.3$
400	22	$4 \cdot 45 \pm 0.0$	$4 \cdot 25 \pm 0.1$	$1 \cdot 06 \pm 0.2$	$2 \cdot 58 \pm 0.1$	$3 \cdot 15 \pm 0.2$	$8 \cdot 48 \pm 0.2$	$4 \cdot 97 \pm 0.2$	$2 \cdot 94 \pm 0.1$	$6 \cdot 40 \pm 0.3$
400	23	$4 \cdot 46 \pm 0.0$	$4 \cdot 56 \pm 0.1$	$1 \cdot 14 \pm 0.2$	$2 \cdot 77 \pm 0.1$	$3 \cdot 39 \pm 0.2$	$9 \cdot 11 \pm 0.2$	$5 \cdot 33 \pm 0.2$	$2 \cdot 19 \pm 0.1$	$6 \cdot 87 \pm 0.3$
500	14	$1 \cdot 02 \pm 0.1$	$8 \cdot 28 \pm 0.2$	$2 \cdot 61 \pm 0.2$	$6 \cdot 33 \pm 0.3$	$4 \cdot 52 \pm 0.2$	$6 \cdot 27 \pm 0.2$	$1 \cdot 22 \pm 0.5$	$2 \cdot 92 \pm 0.5$	$4 \cdot 73 \pm 0.7$
500	15	$1 \cdot 03 \pm 0.1$	$8 \cdot 29 \pm 0.2$	$2 \cdot 62 \pm 0.2$	$6 \cdot 36 \pm 0.3$	$4 \cdot 53 \pm 0.2$	$6 \cdot 29 \pm 0.2$	$1 \cdot 22 \pm 0.5$	$2 \cdot 93 \pm 0.5$	$4 \cdot 75 \pm 0.7$
500	16	$1 \cdot 09 \pm 0.1$	$8 \cdot 32 \pm 0.2$	$2 \cdot 74 \pm 0.2$	$6 \cdot 66 \pm 0.3$	$4 \cdot 64 \pm 0.2$	$6 \cdot 46 \pm 0.2$	$1 \cdot 28 \pm 0.5$	$3 \cdot 00 \pm 0.5$	$4 \cdot 87 \pm 0.7$
500	17	$1 \cdot 76 \pm 0.1$	$8 \cdot 73 \pm 0.2$	$3 \cdot 94 \pm 0.2$	$9 \cdot 58 \pm 0.3$	$5 \cdot 80 \pm 0.2$	$8 \cdot 29 \pm 0.2$	$1 \cdot 84 \pm 0.5$	$3 \cdot 75 \pm 0.5$	$6 \cdot 25 \pm 0.7$
500	18	$7 \cdot 49 \pm 0.1$	$1 \cdot 30 \pm 0.1$	$1 \cdot 60 \pm 0.1$	$3 \cdot 88 \pm 0.2$	$2 \cdot 08 \pm 0.1$	$3 \cdot 65 \pm 0.1$	$7 \cdot 47 \pm 0.5$	$1 \cdot 34 \pm 0.4$	$2 \cdot 98 \pm 0.6$
500	19	$2 \cdot 88 \pm 0.0$	$6 \cdot 08 \pm 0.1$	$1 \cdot 37 \pm 0.0$	$3 \cdot 32 \pm 0.1$	$3 \cdot 02 \pm 0.0$	$9 \cdot 13 \pm 0.0$	$6 \cdot 39 \pm 0.4$	$1 \cdot 95 \pm 0.3$	$6 \cdot 13 \pm 0.5$
500	20	$4 \cdot 24 \pm 0.0$	$5 \cdot 07 \pm 0.0$	$1 \cdot 26 \pm 0.1$	$3 \cdot 06 \pm 0.0$	$3 \cdot 63 \pm 0.1$	$9 \cdot 95 \pm 0.1$	$5 \cdot 89 \pm 0.3$	$2 \cdot 35 \pm 0.2$	$7 \cdot 51 \pm 0.4$
500	21	$4 \cdot 49 \pm 0.0$	$2 \cdot 67 \pm 0.1$	$6 \cdot 71 \pm 0.1$	$1 \cdot 63 \pm 0.1$	$2 \cdot 00 \pm 0.2$	$5 \cdot 41 \pm 0.2$	$3 \cdot 14 \pm 0.2$	$1 \cdot 29 \pm 0.1$	$4 \cdot 04 \pm 0.3$
500	22	$4 \cdot 55 \pm 0.0$	$4 \cdot 65 \pm 0.1$	$1 \cdot 17 \pm 0.2$	$2 \cdot 84 \pm 0.1$	$3 \cdot 50 \pm 0.2$	$9 \cdot 46 \pm 0.2$	$5 \cdot 47 \pm 0.2$	$2 \cdot 26 \pm 0.1$	$7 \cdot 14 \pm 0.3$
500	23	$4 \cdot 56 \pm 0.0$	$5 \cdot 02 \pm 0.1$	$1 \cdot 26 \pm 0.2$	$3 \cdot 07 \pm 0.1$	$3 \cdot 79 \pm 0.2$	$1 \cdot 02 \pm 0.3$	$5 \cdot 91 \pm 0.2$	$2 \cdot 44 \pm 0.1$	$7 \cdot 71 \pm 0.3$

TABLE 12

## ZINC XX

INTENSITY RATIO  $I(\text{H}\ \text{L} + \text{I}\ \text{I}\ \text{I})/I(\text{3P} - \text{3S})$ 

T(EV)	L	G	N	3D-3P	4S-3P	4P-3S	4P-3D	4D-3P	4F-3D	4F-4S	4G-4P	4F-4I
50	14	3.41-02	5.18-04	7.00-05	1.51-05	1.31-04	1.59-04	1.65-08	3.65-08	1.19-09		
50	15	3.43-02	5.18-04	7.06-05	1.52-05	1.31-04	1.67-04	1.67-08	3.65-08	1.20-09		
50	16	3.69-02	5.21-04	7.63-05	1.64-05	1.34-04	1.64-04	1.80-08	3.74-08	1.23-09		
50	17	6.19-02	5.46-04	1.34-04	2.68-05	1.65-04	2.08-04	3.16-08	4.61-08	1.56-09		
50	18	2.68-01	6.08-04	7.12-04	1.53-04	6.04-04	9.57-04	1.68-07	7.18-09			
50	19	9.31-01	3.61-03	6.50-03	1.41-03	9.11-03	1.79-02	1.53-06	2.54-06	1.34-07		
50	20	1.29-00	2.77-02	5.71-02	1.23-02	1.07-01	2.20-01	1.35-05	2.99-05	1.45-06		
50	21	1.34-00	1.57-01	3.33-01	7.17-02	6.68-01	1.42-00	7.08-05	1.87-04	1.16-05		
50	22	1.34-00	3.16-01	6.76-01	1.45-01	1.37-00	2.92-01	1.60-04	3.42-04	2.19-05		
50	23	1.34-00	3.53-01	7.54-01	1.62-01	1.53-00	3.26-00	1.78-04	4.26-04	2.44-05		
100	14	5.96-02	9.32-03	1.71-03	3.67-04	3.65-03	4.83-03	4.03-07	1.02-06	3.62-08		
100	15	6.10-02	9.33-03	1.72-03	3.69-04	3.65-03	4.84-03	4.06-07	1.02-06	3.63-08		
100	16	6.34-02	9.36-03	1.81-03	3.89-04	3.71-03	4.93-03	4.28-07	1.04-06	3.70-08		
100	17	9.68-02	9.70-03	2.75-03	5.91-04	4.37-03	5.94-03	6.49-07	1.22-06	4.46-08		
100	18	3.86-01	1.32-02	1.21-02	2.61-03	1.29-02	2.15-02	2.87-06	3.59-06	1.61-07		
100	19	1.52-00	5.06-02	1.06-01	2.28-02	1.76-01	3.88-01	2.50-05	4.92-05	2.91-06		
100	20	2.20-00	3.85-01	9.51-01	2.05-01	2.20-00	5.13-00	2.25-04	6.15-04	3.65-05		
100	21	2.42-00	2.43-00	6.23-00	1.34-00	1.55-01	3.70-01	1.47-03	4.34-03	2.77-04		
100	22	2.43-00	5.76-01	1.48-01	3.18-00	3.73-01	8.91-01	3.50-03	1.04-02	6.68-04		
100	23	2.44-00	6.08-00	1.72-01	3.69-00	4.33-01	1.04-02	4.06-03	1.21-02	7.77-04		

TABLE 13

## ZINC XX

INTENSITY RATIO  $I(\text{H}_\alpha, \text{L} - \text{H}'_\alpha)/I(3\text{P} - 3\text{S})$ 

T(EV)	L <sub>NG</sub>	H	3P-3P	4S-3P	4P-3S	4P-3D	4D-3P	4F-3P	4P-4S	4D-4P	4F-4P
150	14	7.19-02	2.39-02	5.15-03	1.11-03	1.10-02	1.47-02	1.22-06	3.08-06	1.11-07	
150	15	7.23-02	2.39-02	5.17-03	1.11-03	1.10-02	1.47-02	1.22-06	3.08-06	1.11-07	
150	16	7.58-02	2.40-02	5.39-03	1.16-03	1.12-02	1.50-02	1.27-06	3.12-06	1.12-07	
150	17	1.10-01	2.47-02	7.59-03	1.63-03	1.29-02	1.76-02	1.79-06	3.61-06	1.32-07	
150	18	4.10-01	3.20-02	2.96-02	6.36-03	3.42-02	5.68-02	6.98-06	9.56-06	4.26-07	
150	19	1.73+00	1.15-01	2.49-01	5.36-02	4.34-01	9.89-01	5.89-05	1.21-04	7.42-06	
150	20	2.76+00	8.66-01	2.26+00	4.87-01	5.61+00	1.36+01	5.35-04	1.56-03	1.62-04	
150	21	2.94+00	5.76+00	1.57+01	3.37+00	4.20+01	1.04+02	3.70-03	1.17-02	7.40-04	
150	22	2.97+00	1.49+01	4.08+01	8.77+00	1.10+02	2.74+02	9.63-03	3.08-02	2.16-03	
150	23	2.97+00	1.78+01	4.86+01	1.04+01	1.32+02	3.27+02	1.15-02	3.68-02	2.46-03	
200	14	7.91-02	3.78-02	9.16-03	1.97-03	1.91-02	2.54-02	2.17-06	5.34-06	1.91-07	
200	15	7.75-02	3.78-02	9.19-03	1.98-03	1.91-02	2.54-02	2.17-06	5.34-06	1.91-07	
200	16	8.30-02	3.79-02	9.51-03	2.05-03	1.94-02	2.58-02	2.25-06	5.42-06	1.94-07	
200	17	1.17-01	3.90-02	1.27-02	2.74-03	2.21-02	2.70-02	3.01-06	6.17-06	2.25-07	
200	18	4.23-01	5.60-02	4.50-02	9.69-03	5.50-02	8.66-02	1.06-05	1.53-05	6.72-07	
200	19	1.62+00	1.68-01	3.70-01	7.95-02	6.55-01	1.52+00	8.74-05	1.83-04	1.14-05	
200	20	3.62+00	1.26+00	3.38+00	7.28-01	8.64+00	2.15+01	7.69-04	2.41-03	1.61-04	
200	21	3.24+00	8.64+00	2.42+01	5.21+00	6.73+01	1.70+02	5.72-03	1.86-02	1.27-03	
200	22	3.27+00	2.38+01	6.71+01	1.44+01	1.89+02	4.77+02	1.59-02	5.26-02	3.58-03	
200	23	3.24+00	2.80+01	8.17+01	1.76+01	2.30+02	5.82+02	1.93-02	6.41-02	4.36-03	

TABLE 14

ZINC XX

INTENSITY RATIO  $I(11L - 11'L')/I(3P - 3S)$ 

T(EV)	LNG	4S-3P	4S-3S	4P-3D	4P-3P	4F-3P	4P-4S	4D-4P	4F-4P	
300	14	8.72+02	5.89+02	1.67+02	3.60+03	3.32+02	4.31+02	3.94+06	9.25+06	3.24+07
300	15	8.75+02	5.89+02	1.68+02	3.61+03	3.32+02	4.32+02	3.97+06	9.28+06	3.24+07
300	16	9.08+02	5.91+02	1.72+02	3.71+03	3.36+02	4.36+02	4.07+06	9.39+06	3.78+07
300	17	1.23+01	6.06+02	2.17+02	4.67+03	3.78+02	4.99+02	5.13+06	1.65+05	3.74+07
300	18	4.10+01	7.57+02	6.68+02	1.44+02	8.67+02	1.36+01	1.58+05	2.42+05	1.12+06
300	19	1.68+00	2.38+01	5.23+01	1.12+01	9.40+01	2.20+00	1.24+04	2.62+04	1.65+05
300	20	3.29+00	1.76+00	4.83+00	1.04+00	1.27+01	3.25+01	1.14+03	3.54+03	2.04+04
300	21	3.57+00	1.25+01	3.61+01	7.77+00	1.04+02	2.68+02	8.54+03	2.97+02	2.11+03
300	22	3.61+00	3.75+01	1.09+02	2.35+01	3.18+02	8.21+02	2.58+02	8.88+02	6.11+03
300	23	3.62+00	4.71+01	1.37+02	2.95+01	4.06+02	1.03+03	3.24+02	1.11+01	7.74+03
400	14	9.15+02	7.29+02	2.30+02	4.95+03	4.38+02	5.57+02	5.44+06	1.22+05	4.18+07
400	15	9.16+02	7.29+02	2.30+02	4.96+03	4.38+02	5.58+02	5.45+06	1.22+05	4.18+07
400	16	9.49+02	7.31+02	2.36+02	5.07+03	4.43+02	5.65+02	5.57+06	1.24+05	4.24+07
400	17	1.26+01	7.48+02	2.86+02	6.16+03	4.94+02	6.37+02	6.77+06	1.38+05	4.74+07
400	18	4.08+01	9.20+02	7.98+02	1.72+02	1.07+01	1.63+01	1.89+05	3.00+05	1.22+06
400	19	1.88+00	2.76+01	6.01+01	1.29+01	1.09+00	2.54+00	1.42+04	3.03+04	1.01+05
400	20	3.42+00	2.01+00	5.59+00	1.20+00	1.49+01	3.86+01	1.32+03	4.15+03	2.90+04
400	21	3.74+00	1.47+01	4.30+01	9.25+00	1.26+02	3.28+02	1.02+02	3.52+02	2.46+03
400	22	3.79+00	4.67+01	1.38+02	2.97+01	4.09+02	1.07+03	3.26+02	1.14+01	8.10+03
400	23	3.80+00	6.00+01	1.77+02	3.81+01	5.27+02	1.37+03	4.19+02	1.47+01	1.43+02

TABLE 15

ZINC XX		INTENSITY RATIO $I(^n\text{L} - ^{n+1}\text{L})/I(^3\text{P} - ^3\text{S})$									
T(EV)	LNG N	3P-3P	4S-3P	4D-3S	4P-3D	4D-3P	4F-3D	4P-4S	4G-4P	4F-4D	
500	14	9.41-02	8.25-02	2.80-02	6.03-03	5.17-02	6.47-02	6.62-06	1.44-05	4.45-07	
500	15	9.44-02	8.25-02	2.81-02	6.04-03	5.18-02	6.47-02	6.63-06	1.44-05	4.46-07	
500	16	9.73-02	8.27-02	2.86-02	6.15-03	5.23-02	6.55-02	6.76-06	1.46-05	4.91-07	
500	17	1.27-01	8.45-02	3.40-02	7.31-03	5.79-02	7.33-02	8.03-06	1.62-05	5.51-07	
500	18	3.96-01	1.93-01	6.79-02	1.80-02	1.21-01	1.79-01	2.08-05	3.38-05	1.44-06	
500	19	1.36-00	2.97-01	6.39-01	1.38-01	1.16-00	2.70-00	1.51-04	3.25-04	2.13-05	
500	20	3.50-00	2.14-01	5.97-00	1.28-00	1.60-01	4.20-01	1.41-03	4.46-03	3.15-04	
500	21	3.85-00	1.59-01	4.69-01	1.01-01	1.39-02	3.64-02	1.11-02	3.88-02	2.73-03	
500	22	3.91-00	5.29-01	1.58-02	3.39-01	4.73-02	1.24-03	3.72-02	1.32-01	9.31-03	
500	23	3.92-00	6.93-01	2.07-02	4.44-01	6.21-02	1.63-03	4.86-02	1.73-01	1.22-02	
600	14	9.58-12	N.95-02	3.20-02	6.69-03	5.78-02	7.13-02	7.57-06	1.61-05	5.35-07	
600	15	9.01-02	8.95-02	3.21-02	6.90-03	5.78-02	7.14-02	7.58-06	1.61-05	5.35-07	
600	16	9.89-02	8.97-02	3.26-02	7.02-03	5.84-02	7.21-02	7.71-06	1.63-05	5.41-07	
600	17	1.27-01	9.15-02	3.61-02	8.20-03	6.43-02	8.02-02	9.00-06	1.80-05	6.12-07	
600	18	3.65-01	1.10-01	9.30-02	2.09-02	1.31-01	1.88-01	2.20-05	3.64-05	1.41-06	
600	19	1.83-00	3.09-01	6.57-01	1.41-01	1.19-00	2.76-00	1.55-04	3.32-04	2.07-05	
600	20	3.54-00	2.20-00	6.16-00	1.32-00	1.65-01	4.38-01	1.45-03	4.61-03	3.28-04	
600	21	3.92-00	1.65-01	4.91-01	1.06-01	1.46-02	3.86-02	1.16-02	4.09-02	2.90-03	
600	22	3.98-00	5.72-01	1.72-02	3.69-01	5.16-02	1.36-03	4.05-02	1.45-01	1.02-02	
600	23	4.60-00	7.62-01	2.29-02	4.92-01	6.92-02	1.82-03	5.41-02	1.93-01	1.37-02	

TABLE 16

ZINC XX

INTENSITY RATIO I(U, L - H'L')/I(3P - 3S)

T(EV)	LOG N	3L-3P	4S-3P	4P-3S	4P-3D	4I-3P	4F-3P	4P-4S	4I-4P	4F-4D
800	14	9.80-02	9.87-02	3.80-02	8.18-03	6.64-02	8.03-02	8.09-06	1.85-05	6.02-07
800	15	9.83-02	9.87-02	3.81-02	8.19-03	6.65-02	8.14-02	9.00-06	1.86-05	6.03-07
800	16	1.01-01	9.89-02	3.86-02	8.31-03	6.71-02	8.12-02	9.13-06	1.87-05	6.04-07
800	17	1.26-01	1.01-01	4.41-02	9.48-03	7.33-02	8.74-02	1.04-05	2.15-05	6.71-07
800	18	3.65-01	1.19-01	9.87-02	2.12-02	1.42-01	1.42-01	2.33-05	3.96-05	1.48-10
800	19	1.76-00	3.10-01	6.62-01	1.42-01	1.20-00	2.73-00	1.56-04	3.35-04	2.65-05
800	20	3.58-00	2.23-00	6.23-00	1.34-00	1.34-00	1.67-01	4.48-01	1.47-03	3.36-04
800	21	6.01-00	1.70-01	5.09-01	1.09-01	1.53-02	4.66-02	1.20-02	4.27-02	3.65-03
800	22	4.04-00	6.25-01	1.89-02	4.06-01	5.76-02	1.52-03	4.46-02	1.61-01	1.14-02
800	23	4.10-00	8.58-01	2.59-02	5.58-01	7.92-02	2.19-03	6.13-02	2.21-01	1.57-02
1000	14	9.94-02	1.05-01	4.22-02	9.09-03	7.23-02	8.61-02	9.98-06	2.02-05	6.46-07
1000	15	9.96-02	1.05-01	4.23-02	9.10-03	7.23-02	8.62-02	10.60-06	2.02-05	6.47-07
1000	16	1.02-01	1.05-01	4.28-02	9.21-03	7.30-02	8.70-02	1.01-05	2.04-05	6.53-07
1000	17	1.26-01	1.07-01	4.81-02	1.03-02	7.92-02	9.51-02	1.14-05	2.21-05	7.14-07
1000	18	3.49-01	1.25-01	1.01-01	2.18-02	1.48-01	2.00-01	2.39-05	4.12-15	1.56-08
1000	19	1.70-00	3.19-01	6.51-01	1.40-01	1.18-00	2.64-00	1.54-04	3.28-04	1.98-05
1000	20	3.60-00	2.29-00	6.13-00	1.32-00	1.64-01	4.43-01	1.45-03	4.59-03	3.33-04
1000	21	4.06-00	1.70-01	5.10-01	1.10-01	1.54-02	4.16-02	1.20-02	4.29-02	3.08-03
1000	22	4.14-00	6.54-01	1.98-02	4.27-01	6.08-02	1.61-03	4.69-02	1.70-01	1.21-02
1000	23	4.16-00	9.20-01	2.79-02	6.01-01	8.58-02	2.27-03	6.60-02	2.39-01	1.71-02

TABLE 17

## KEYPTON XXVI

INTENSITY RATIO  $I(^nL - ^{n'L})/I(^3P - ^3S)$ 

T(EV)	LOG N	3P-3P	4S-3P	4P-3S	4P-3P	4D-3P	4P-4S	4C-4P	4F-4P
50	15	2.17-02	1.34-05	1.84-06	3.41-07	2.99-06	2.05-10	3.36-11	1.29-11
50	16	2.23-02	1.34-05	1.89-06	3.49-07	3.02-06	2.56-10	2.10-10	3.39-11
50	17	2.32-02	1.36-05	2.32-06	4.35-07	3.26-06	2.65-10	2.62-10	3.66-11
50	18	2.42-02	1.61-05	7.01-06	1.30-06	6.11-06	6.43-06	7.81-10	6.87-10
50	19	3.56-01	4.16-05	5.56-05	1.03-05	5.51-05	9.00-05	6.19-09	6.19-09
50	20	6.36-01	2.74-04	5.41-04	1.00-04	7.54-04	1.35-03	6.93-08	8.47-08
50	21	6.84-01	1.96-03	4.37-03	8.10-04	7.11-03	1.30-02	4.97-07	7.99-07
50	22	6.90-01	6.05-03	1.84-02	3.42-03	3.12-02	5.86-02	2.06-06	3.51-06
50	23	6.91-01	1.21-02	2.77-02	5.13-03	4.71-02	8.87-02	3.09-06	5.29-06
50	24	6.91-01	1.27-02	2.92-02	5.40-03	4.96-02	9.35-02	3.25-06	5.57-06
100	15	4.54-02	1.65-03	3.18-04	5.89-05	6.55-04	7.41-04	3.55-08	7.36-09
100	16	4.63-02	1.65-03	3.24-04	5.99-05	6.59-04	7.46-04	3.61-08	7.40-09
100	17	5.58-02	1.67-03	3.79-04	7.01-05	6.99-04	7.90-04	4.22-08	7.85-09
100	18	1.44-01	1.89-03	9.31-04	1.72-04	1.14-03	1.46-03	1.04-07	1.29-07
100	19	6.60-01	4.17-03	6.63-03	1.23-03	8.40-03	1.59-02	7.39-07	9.44-07
100	20	1.33-00	2.54-02	6.37-02	1.18-02	1.18-01	2.54-01	7.09-06	1.32-05
100	21	1.49-00	1.66-01	5.35-01	9.00-02	1.17-00	2.57-00	5.96-05	1.31-04
100	22	1.51-00	8.98-01	2.66-00	4.93-01	6.64-00	1.35-01	2.97-04	6.79-04
100	23	1.51-00	1.52-00	4.53-00	8.38-01	1.03-01	2.31-01	5.05-04	1.16-03
100	24	1.51-00	1.64-00	4.87-00	9.02-01	1.11-01	2.49-01	5.43-04	1.25-03

TABLE 1A

## KRYPTON XXVI

INTENSITY RATIO  $I(^nL - ^{n'}L') / I(^nP - ^{nP})$ 

T(KEV)	LOG N	3D-3P	4S-3P	4F-3S	4P-3D	4C-3P	4P-4S	4F-4P	4F-4I
200	15	6.49-02	1.77-02	4.44-03	8.23-04	9.58-03	1.14-02	4.95-07	1.08-00
200	16	6.64-02	1.77-02	4.49-03	8.32-04	9.63-03	1.14-02	5.01-07	1.09-00
200	17	7.64-02	1.79-02	5.00-03	9.26-04	1.01-02	1.21-02	5.57-07	1.13-00
200	18	1.75-01	1.96-02	1.01-02	1.87-03	1.49-02	1.95-02	1.13-06	1.68-00
200	19	6.21-01	3.79-02	6.26-02	1.16-02	8.87-02	1.74-01	6.97-06	9.97-00
200	20	1.89-00	2.13-01	5.93-01	1.19-01	1.24-00	2.96-01	6.61-05	1.40-04
200	21	2.19-00	1.58-00	5.15-00	9.53-01	1.30-01	3.12-01	5.74-04	1.46-03
200	22	2.23-00	8.69-00	2.93-01	5.42-00	7.69-01	1.87-02	3.26-03	8.64-03
200	23	2.23-00	1.68-01	5.68-01	1.05-01	1.50-02	3.66-02	6.33-03	1.68-02
200	24	2.23-00	1.85-01	6.28-01	1.16-01	1.66-02	4.05-02	6.99-03	1.86-02
300	15	7.34-02	3.81-02	1.12-02	2.07-03	2.33-02	2.76-02	1.24-06	2.62-06
300	16	7.45-02	3.81-02	1.13-02	2.09-03	2.34-02	2.78-02	1.26-06	2.63-06
300	17	8.46-02	3.94-02	1.23-02	2.27-03	2.44-02	2.91-02	1.37-06	2.74-06
300	18	1.81-01	4.17-02	2.21-02	4.10-03	3.46-02	4.44-02	2.47-06	3.89-06
300	19	8.46-01	7.58-02	1.24-01	2.29-02	1.82-01	3.54-01	1.38-05	2.05-05
300	20	2.09-00	4.07-01	1.16-00	2.15-01	2.52-00	6.21-00	1.29-04	2.84-04
300	21	2.48-00	3.13-01	1.03-01	1.99-00	2.70-01	6.73-01	1.14-03	3.04-03
300	22	2.53-00	1.77-01	6.22-01	1.15-01	1.71-02	4.30-02	6.93-03	1.93-02
300	23	2.54-00	3.70-01	1.31-02	2.42-01	3.62-02	9.11-02	1.46-02	4.67-02
300	24	2.54-00	4.16-01	1.47-02	2.72-01	4.08-02	1.02-03	1.64-02	4.58-02

TABLE 19

## CRYPTON XXVI

INTENSITY RATIO  $I(L, L + \Delta L)/[I(3P - 3S)]$ 

T(EV)	LAG	H	3P-3P	4S-3P	4S-3S	4P-3D	4F-3P	4F-3S	4P-4S	4D-4P	4F-4C
400	15	7.83-02	5.53-02	1.81-02	3.35-03	3.64-02	4.24-02	2.02-06	4.09-06	2.05-07	
400	16	7.93-02	5.53-02	1.82-02	3.38-03	3.65-02	4.29-02	2.03-06	4.10-06	2.06-07	
400	17	8.90-02	5.57-02	1.96-02	3.62-03	3.79-02	4.46-02	2.18-06	4.26-06	2.14-07	
400	18	1.82-01	6.01-02	3.28-02	6.07-03	5.24-02	6.59-02	3.65-06	5.49-06	3.17-07	
400	19	8.45-01	1.05-01	1.69-01	3.13-02	2.55-01	4.86-01	1.88-05	2.66-05	2.34-06	
400	20	2.19-00	5.47-01	1.57-00	2.91-01	3.47-00	8.79-00	1.75-04	3.91-04	4.18-05	
400	21	2.64-00	4.97-00	1.40-01	2.60-00	3.78-01	9.58-01	1.56-03	4.25-03	4.61-04	
400	22	2.76-00	2.47-01	8.88-01	1.64-01	2.51-02	6.38-02	9.29-03	2.82-02	3.67-03	
400	23	2.71-00	5.47-01	1.97-02	3.65-01	5.60-02	1.43-03	2.20-02	6.29-02	6.67-03	
400	24	2.71-00	6.23-01	2.25-02	4.16-01	6.39-02	1.63-03	2.50-02	7.18-02	7.83-03	
500	15	8.14-02	6.87-02	2.45-02	4.53-03	4.75-02	5.49-02	2.73-06	5.34-06	2.64-07	
500	16	8.23-02	6.88-02	2.46-02	4.56-03	4.77-02	5.51-02	2.74-06	5.36-06	2.65-07	
500	17	9.16-02	6.93-02	2.62-02	4.84-03	4.94-02	5.73-02	2.91-06	5.55-06	2.75-07	
500	18	1.51-01	7.43-02	4.16-02	7.70-03	6.70-02	8.26-02	4.63-06	7.53-06	3.97-07	
500	19	8.32-01	1.27-01	2.00-01	3.70-02	3.07-01	5.74-01	2.23-05	3.45-05	2.76-06	
500	20	2.24-00	6.42-01	1.84-00	3.41-01	4.14-00	1.94-01	2.05-04	4.62-04	5.01-05	
500	21	2.74-00	4.77-00	1.66-01	3.08-00	4.53-01	1.16-02	1.85-03	5.09-03	5.59-04	
500	22	2.81-00	2.98-01	1.08-02	2.01-01	3.11-02	7.98-02	1.21-02	3.49-02	3.84-03	
500	23	2.82-00	6.98-01	2.51-02	4.65-01	7.25-02	1.86-03	2.80-02	8.14-02	8.96-03	
500	24	2.82-00	7.93-01	2.90-02	5.37-01	8.36-02	2.15-03	3.23-02	9.39-02	1.03-02	

TABLE 20

## KRYPTON XXVI

INTENSITY RATIO  $I(4P_1) - I(4P_3)/I(3P_0 - 3S)$ 

T(EV)	LNG	$4P_1 - 3P_0$	$4S - 3P_0$	$4F - 3S$	$4P - 3D$	$4P - 3P$	$4P - 3D$	$4P - 4S$	$4D - 4P$	$4F - 4P$
750	15	8.54-02	9.12-02	3.72-02	6.89-03	6.79-02	7.62-02	4.15-06	7.63-06	3.56-07
750	16	5.67-02	9.12-02	3.74-02	6.92-03	6.81-02	7.65-02	4.17-06	7.66-06	3.58-07
750	17	9.51-02	9.16-02	3.92-02	7.25-03	7.03-02	7.92-02	4.37-06	7.93-06	3.61-07
750	18	1.76-01	9.77-02	5.72-02	1.76-02	9.25-02	1.10-01	6.37-06	1.01-05	5.27-07
750	19	7.92-01	1.59-01	2.42-01	4.48-02	3.81-01	6.82-01	2.70-05	4.23-05	3.26-06
750	20	2.29+00	7.65-01	2.18+00	4.04-01	4.92+00	1.27+01	2.43-04	5.52-04	6.09-05
750	21	2.87+00	5.69+00	2.80+01	3.71+01	5.54+01	1.45+02	2.23-03	6.23-03	6.97-04
750	22	2.95+00	3.71+01	1.37+02	2.54+01	4.01+02	1.04+03	1.53-02	4.50-02	5.02-03
750	23	2.97+00	9.28+01	3.45+02	6.38+01	1.01+03	2.64+03	3.84-02	1.14-01	1.27-02
750	24	2.97+00	1.69+02	4.06+02	7.52+01	1.20+03	3.11+03	4.53-02	1.34-01	1.50-02
1000	15	6.82-02	1.04-01	4.63-02	8.58-03	8.13-02	8.94-02	5.16-06	9.14-06	4.30-07
1000	16	8.90-02	1.05-01	4.65-02	8.61-03	8.15-02	8.96-02	5.18-06	9.16-06	4.31-07
1000	17	9.67-02	1.15-01	4.84-02	8.65-03	8.39-02	9.25-02	5.39-06	9.43-06	4.55-07
1000	18	1.72-01	1.11-01	6.70-02	1.24-02	1.06-01	1.25-01	7.47-06	1.21-05	5.79-07
1000	19	7.53-01	1.75-01	2.59-01	4.79-02	4.13-01	7.13-01	2.89-05	4.65-05	3.43-06
1000	20	2.29+00	8.11-01	2.29+00	4.24-01	5.17+00	1.34+01	2.55-04	5.81-04	6.34-05
1000	21	2.94+00	6.61+00	2.12+01	3.93+00	5.91+01	1.57+02	2.36-03	6.65-03	7.53-04
1000	22	3.03+00	4.04+01	1.50+02	2.79+01	4.44+02	1.15+03	1.68-02	4.98-02	5.59-03
1000	23	3.05+00	1.07+02	4.01+02	7.42+01	1.19+03	3.11+03	4.46-02	1.34-01	1.50-02
1000	24	3.05+00	1.28+02	4.81+02	8.90+03	1.43+03	3.74+03	5.36-02	1.60-01	1.80-02

TABLE 21

## ΚΡΥΨΤΑΝΙ ΣΣΒΙ

INTENSITY RATIO  $I(H_L) - I(H_I)/I(3P - 3S)$ 

$\tau(\text{EV})$	$\log n$	$3D-3P$	$4S-3P$	$4F-3S$	$4P-3D$	$4D-3P$	$4P-4S$	$4F-3P$	$4F-4D$
125.0	15	$8 \cdot 96 \cdot 10^{-12}$	$1 \cdot 13 \cdot 10^{-11}$	$5 \cdot 30 \cdot 10^{-2}$	$9 \cdot 82 \cdot 10^{-3}$	$9 \cdot 06 \cdot 10^{-2}$	$9 \cdot 81 \cdot 10^{-2}$	$5 \cdot 91 \cdot 10^{-6}$	$1 \cdot 02 \cdot 10^{-5}$
125.0	16	$9 \cdot 04 \cdot 10^{-12}$	$1 \cdot 13 \cdot 10^{-11}$	$5 \cdot 32 \cdot 10^{-2}$	$9 \cdot 85 \cdot 10^{-3}$	$9 \cdot 09 \cdot 10^{-2}$	$9 \cdot 84 \cdot 10^{-2}$	$5 \cdot 93 \cdot 10^{-6}$	$1 \cdot 02 \cdot 10^{-5}$
125.0	17	$9 \cdot 75 \cdot 10^{-12}$	$1 \cdot 14 \cdot 10^{-11}$	$5 \cdot 51 \cdot 10^{-2}$	$1 \cdot 02 \cdot 10^{-2}$	$9 \cdot 53 \cdot 10^{-2}$	$1 \cdot 01 \cdot 10^{-1}$	$6 \cdot 13 \cdot 10^{-6}$	$1 \cdot 05 \cdot 10^{-5}$
125.0	18	$1 \cdot 07 \cdot 10^{-11}$	$1 \cdot 20 \cdot 10^{-11}$	$7 \cdot 37 \cdot 10^{-2}$	$1 \cdot 56 \cdot 10^{-2}$	$1 \cdot 16 \cdot 10^{-1}$	$1 \cdot 34 \cdot 10^{-1}$	$8 \cdot 21 \cdot 10^{-6}$	$1 \cdot 33 \cdot 10^{-5}$
125.0	19	$7 \cdot 19 \cdot 10^{-11}$	$1 \cdot 84 \cdot 10^{-11}$	$2 \cdot 65 \cdot 10^{-1}$	$4 \cdot 91 \cdot 10^{-2}$	$4 \cdot 27 \cdot 10^{-1}$	$7 \cdot 14 \cdot 10^{-1}$	$2 \cdot 95 \cdot 10^{-5}$	$4 \cdot 80 \cdot 10^{-5}$
125.0	20	$2 \cdot 27 \cdot 10^{-10}$	$4 \cdot 24 \cdot 10^{-11}$	$2 \cdot 30 \cdot 10^{-1}$	$4 \cdot 26 \cdot 10^{-1}$	$5 \cdot 21 \cdot 10^{-1}$	$1 \cdot 35 \cdot 10^{-1}$	$2 \cdot 57 \cdot 10^{-4}$	$5 \cdot 85 \cdot 10^{-4}$
125.0	21	$2 \cdot 98 \cdot 10^{-10}$	$6 \cdot 10 \cdot 10^{-11}$	$2 \cdot 15 \cdot 10^{-1}$	$3 \cdot 98 \cdot 10^{-1}$	$6 \cdot 01 \cdot 10^{-1}$	$1 \cdot 66 \cdot 10^{-2}$	$2 \cdot 40 \cdot 10^{-3}$	$6 \cdot 70 \cdot 10^{-3}$
125.0	22	$3 \cdot 68 \cdot 10^{-10}$	$4 \cdot 10 \cdot 10^{-11}$	$1 \cdot 56 \cdot 10^{-2}$	$2 \cdot 90 \cdot 10^{-1}$	$4 \cdot 64 \cdot 10^{-2}$	$1 \cdot 22 \cdot 10^{-3}$	$1 \cdot 74 \cdot 10^{-2}$	$5 \cdot 21 \cdot 10^{-2}$
125.0	23	$3 \cdot 09 \cdot 10^{-10}$	$1 \cdot 16 \cdot 10^{-11}$	$4 \cdot 36 \cdot 10^{-2}$	$8 \cdot 08 \cdot 10^{-1}$	$1 \cdot 30 \cdot 10^{-3}$	$3 \cdot 42 \cdot 10^{-3}$	$4 \cdot 86 \cdot 10^{-2}$	$5 \cdot 87 \cdot 10^{-3}$
125.0	24	$3 \cdot 10 \cdot 10^{-10}$	$1 \cdot 41 \cdot 10^{-12}$	$5 \cdot 32 \cdot 10^{-2}$	$9 \cdot 84 \cdot 10^{-1}$	$1 \cdot 59 \cdot 10^{-3}$	$4 \cdot 17 \cdot 10^{-3}$	$5 \cdot 92 \cdot 10^{-2}$	$1 \cdot 78 \cdot 10^{-1}$
150.0	15	$9 \cdot 06 \cdot 10^{-12}$	$1 \cdot 19 \cdot 10^{-11}$	$5 \cdot 81 \cdot 10^{-2}$	$1 \cdot 08 \cdot 10^{-2}$	$9 \cdot 75 \cdot 10^{-2}$	$1 \cdot 04 \cdot 10^{-1}$	$6 \cdot 47 \cdot 10^{-6}$	$1 \cdot 09 \cdot 10^{-5}$
150.0	16	$9 \cdot 13 \cdot 10^{-12}$	$1 \cdot 10 \cdot 10^{-11}$	$5 \cdot 83 \cdot 10^{-2}$	$1 \cdot 08 \cdot 10^{-2}$	$9 \cdot 77 \cdot 10^{-2}$	$1 \cdot 05 \cdot 10^{-1}$	$6 \cdot 49 \cdot 10^{-6}$	$1 \cdot 10 \cdot 10^{-5}$
150.0	17	$9 \cdot 89 \cdot 10^{-12}$	$1 \cdot 20 \cdot 10^{-11}$	$6 \cdot 01 \cdot 10^{-2}$	$1 \cdot 11 \cdot 10^{-2}$	$1 \cdot 00 \cdot 10^{-1}$	$1 \cdot 07 \cdot 10^{-1}$	$6 \cdot 70 \cdot 10^{-6}$	$1 \cdot 13 \cdot 10^{-5}$
150.0	18	$1 \cdot 03 \cdot 10^{-11}$	$1 \cdot 26 \cdot 10^{-11}$	$7 \cdot 84 \cdot 10^{-2}$	$1 \cdot 45 \cdot 10^{-2}$	$1 \cdot 25 \cdot 10^{-1}$	$1 \cdot 39 \cdot 10^{-1}$	$8 \cdot 74 \cdot 10^{-6}$	$1 \cdot 41 \cdot 10^{-5}$
150.0	19	$6 \cdot 06 \cdot 10^{-11}$	$1 \cdot 89 \cdot 10^{-11}$	$2 \cdot 66 \cdot 10^{-1}$	$4 \cdot 93 \cdot 10^{-2}$	$4 \cdot 32 \cdot 10^{-1}$	$7 \cdot 03 \cdot 10^{-1}$	$2 \cdot 97 \cdot 10^{-5}$	$4 \cdot 85 \cdot 10^{-5}$
150.0	20	$2 \cdot 25 \cdot 10^{-10}$	$8 \cdot 23 \cdot 10^{-11}$	$2 \cdot 28 \cdot 10^{-1}$	$4 \cdot 21 \cdot 10^{-1}$	$5 \cdot 14 \cdot 10^{-1}$	$1 \cdot 33 \cdot 10^{-1}$	$2 \cdot 54 \cdot 10^{-4}$	$5 \cdot 78 \cdot 10^{-4}$
150.0	21	$3 \cdot 00 \cdot 10^{-10}$	$6 \cdot 07 \cdot 10^{-11}$	$2 \cdot 14 \cdot 10^{-1}$	$3 \cdot 96 \cdot 10^{-1}$	$5 \cdot 99 \cdot 10^{-1}$	$1 \cdot 61 \cdot 10^{-2}$	$2 \cdot 36 \cdot 10^{-3}$	$6 \cdot 73 \cdot 10^{-3}$
150.0	22	$3 \cdot 11 \cdot 10^{-10}$	$4 \cdot 23 \cdot 10^{-11}$	$1 \cdot 59 \cdot 10^{-2}$	$2 \cdot 94 \cdot 10^{-1}$	$4 \cdot 72 \cdot 10^{-2}$	$1 \cdot 25 \cdot 10^{-3}$	$1 \cdot 77 \cdot 10^{-2}$	$5 \cdot 30 \cdot 10^{-2}$
150.0	23	$3 \cdot 13 \cdot 10^{-10}$	$1 \cdot 22 \cdot 10^{-11}$	$4 \cdot 60 \cdot 10^{-2}$	$8 \cdot 51 \cdot 10^{-1}$	$1 \cdot 38 \cdot 10^{-3}$	$3 \cdot 63 \cdot 10^{-3}$	$5 \cdot 12 \cdot 10^{-2}$	$1 \cdot 55 \cdot 10^{-1}$
150.0	24	$3 \cdot 13 \cdot 10^{-10}$	$1 \cdot 50 \cdot 10^{-12}$	$5 \cdot 68 \cdot 10^{-2}$	$1 \cdot 05 \cdot 10^{-3}$	$4 \cdot 49 \cdot 10^{-3}$	$6 \cdot 33 \cdot 10^{-2}$	$1 \cdot 91 \cdot 10^{-1}$	$2 \cdot 16 \cdot 10^{-2}$

TABLE 22

## MOLYBDENUM XXXII

INTENSITY RATIO  $I(4P - 3S) / I(3P - 3S)$ 

T(FV)	L <sub>G</sub>	$3F - 3P$	$4S - 3P$	$4P - 3S$	$4P - 3D$	$4I - 3P$	$4F - 3S$	$4P - 4S$	$4I - 4P$	$4F - 4D$
100	15	$3.46 \pm 0.2$	$1.64 \pm 0.4$	$2.66 \pm 0.5$	$5.31 \pm 0.6$	$5.71 \pm 0.5$	$5.96 \pm 0.5$	$2.19 \pm 0.9$	$3.33 \pm 0.9$	$2.15 \pm 1.0$
100	16	$3.49 \pm 0.2$	$1.64 \pm 0.4$	$2.68 \pm 0.5$	$5.35 \pm 0.6$	$5.73 \pm 0.5$	$5.96 \pm 0.5$	$2.21 \pm 0.9$	$3.34 \pm 0.9$	$2.15 \pm 1.0$
100	17	$3.74 \pm 0.2$	$1.65 \pm 0.4$	$2.88 \pm 0.5$	$5.74 \pm 0.6$	$5.88 \pm 0.5$	$6.14 \pm 0.5$	$2.37 \pm 0.9$	$3.43 \pm 0.9$	$2.72 \pm 1.0$
100	18	$6.02 \pm 0.2$	$1.71 \pm 0.4$	$4.86 \pm 0.5$	$9.69 \pm 0.6$	$7.45 \pm 0.5$	$8.13 \pm 0.5$	$4.60 \pm 0.9$	$4.34 \pm 0.9$	$2.94 \pm 1.0$
100	19	$2.75 \pm 0.1$	$2.68 \pm 0.4$	$2.51 \pm 0.4$	$5.00 \pm 0.5$	$2.92 \pm 0.4$	$4.45 \pm 0.4$	$2.06 \pm 0.8$	$1.71 \pm 0.8$	$1.41 \pm 0.9$
100	20	$7.42 \pm 0.1$	$1.26 \pm 0.3$	$2.31 \pm 0.3$	$4.61 \pm 0.4$	$3.83 \pm 0.3$	$7.62 \pm 0.3$	$1.90 \pm 0.7$	$2.23 \pm 0.7$	$2.75 \pm 0.8$
100	21	$9.12 \pm 0.1$	$9.78 \pm 0.3$	$2.04 \pm 0.2$	$4.07 \pm 0.3$	$4.39 \pm 0.2$	$8.78 \pm 0.2$	$1.68 \pm 0.6$	$2.56 \pm 0.6$	$3.17 \pm 0.7$
100	22	$9.34 \pm 0.1$	$6.56 \pm 0.2$	$1.43 \pm 0.1$	$2.86 \pm 0.2$	$3.43 \pm 0.1$	$7.08 \pm 0.1$	$1.18 \pm 0.5$	$2.00 \pm 0.5$	$2.56 \pm 0.6$
100	23	$9.36 \pm 0.1$	$1.92 \pm 0.1$	$4.23 \pm 0.1$	$8.45 \pm 0.2$	$1.03 \pm 0.0$	$2.15 \pm 0.0$	$3.48 \pm 0.5$	$6.92 \pm 0.5$	$7.77 \pm 0.6$
100	24	$0.36 \pm 0.1$	$2.40 \pm 0.1$	$5.29 \pm 0.1$	$1.05 \pm 0.1$	$1.29 \pm 0.0$	$2.71 \pm 0.0$	$4.35 \pm 0.5$	$7.54 \pm 0.5$	$9.74 \pm 0.6$
200	15	$5.43 \pm 0.2$	$5.85 \pm 0.3$	$1.25 \pm 0.3$	$2.49 \pm 0.4$	$3.01 \pm 0.3$	$3.46 \pm 0.3$	$1.03 \pm 0.7$	$1.75 \pm 0.7$	$1.25 \pm 0.8$
200	16	$5.47 \pm 0.2$	$5.86 \pm 0.3$	$1.26 \pm 0.3$	$2.51 \pm 0.4$	$3.01 \pm 0.3$	$3.47 \pm 0.3$	$1.03 \pm 0.7$	$1.76 \pm 0.7$	$1.25 \pm 0.8$
200	17	$5.82 \pm 0.2$	$5.98 \pm 0.3$	$1.32 \pm 0.3$	$2.63 \pm 0.4$	$3.07 \pm 0.3$	$3.55 \pm 0.3$	$1.08 \pm 0.7$	$1.79 \pm 0.7$	$1.28 \pm 0.8$
200	18	$9.27 \pm 0.2$	$6.12 \pm 0.3$	$1.95 \pm 0.3$	$3.89 \pm 0.4$	$3.69 \pm 0.3$	$4.39 \pm 0.3$	$1.60 \pm 0.7$	$2.15 \pm 0.7$	$1.59 \pm 0.8$
200	19	$3.06 \pm 0.1$	$8.61 \pm 0.3$	$6.36 \pm 0.3$	$1.67 \pm 0.3$	$1.17 \pm 0.2$	$1.86 \pm 0.2$	$6.88 \pm 0.7$	$6.81 \pm 0.7$	$6.73 \pm 0.8$
200	20	$1.13 \pm 0.0$	$3.52 \pm 0.2$	$7.39 \pm 0.2$	$1.47 \pm 0.2$	$1.43 \pm 0.1$	$3.20 \pm 0.1$	$6.08 \pm 0.6$	$8.35 \pm 0.6$	$1.16 \pm 0.6$
200	21	$1.44 \pm 0.0$	$2.68 \pm 0.1$	$6.59 \pm 0.1$	$1.32 \pm 0.1$	$1.69 \pm 0.0$	$3.87 \pm 0.0$	$5.42 \pm 0.5$	$9.86 \pm 0.5$	$1.40 \pm 0.5$
200	22	$1.53 \pm 0.0$	$1.91 \pm 0.0$	$4.94 \pm 0.0$	$9.86 \pm 0.1$	$1.43 \pm 0.1$	$3.32 \pm 0.1$	$4.07 \pm 0.4$	$8.32 \pm 0.4$	$1.20 \pm 0.4$
200	23	$1.53 \pm 0.0$	$6.03 \pm 0.0$	$3.47 \pm 0.0$	$3.47 \pm 0.0$	$5.12 \pm 0.1$	$1.21 \pm 0.2$	$1.43 \pm 0.3$	$2.98 \pm 0.3$	$4.34 \pm 0.4$
200	24	$1.53 \pm 0.0$	$8.92 \pm 0.0$	$2.34 \pm 0.1$	$4.66 \pm 0.0$	$6.90 \pm 0.1$	$1.62 \pm 0.2$	$1.92 \pm 0.3$	$4.02 \pm 0.3$	$5.87 \pm 0.4$

TABLE 23

## MOLYBDENUM XXXII

INTENSITY RATIO  $I(\text{M'L} - \text{M'L}')/I(\text{3P} - \text{3S})$ 

T(EV)	LOG N	3D-3P	4S-3P	4P-3S	4P-3D	4F-3P	4F-3D	4F-4S	4P-4F	4F-4P
300	15	6.30+02	1.89+02	4.67+03	9.32+04	1.12+02	1.31+02	3.84+07	6.54+07	4.74+08
300	16	6.34+02	1.89+02	4.69+03	9.36+04	1.12+02	1.32+02	3.86+07	6.55+07	4.75+08
300	17	6.60+02	1.96+02	4.87+03	9.72+04	1.14+02	1.34+02	4.01+07	6.66+07	4.84+08
300	18	1.01+01	1.96+02	6.71+03	1.34+03	1.34+02	1.61+02	5.52+07	7.81+07	5.22+08
300	19	3.84+01	2.65+02	2.54+02	5.07+03	3.80+02	6.01+02	2.09+06	2.22+06	2.17+07
300	20	1.27+00	1.60+01	2.17+01	4.34+02	4.41+01	1.62+00	1.79+05	2.57+05	3.65+06
300	21	1.73+00	7.54+01	1.95+00	3.90+01	5.29+00	1.27+01	1.61+04	3.09+04	4.59+05
300	22	1.80+00	5.51+00	1.51+01	3.01+00	4.63+01	1.47+02	1.24+03	2.71+03	4.06+04
300	23	1.81+00	2.16+01	5.83+01	1.16+01	1.83+02	4.47+02	4.79+03	1.96+02	1.61+03
300	24	1.81+00	2.96+01	8.23+01	1.64+01	2.59+02	6.34+02	6.77+03	1.51+02	2.29+03
400	15	6.81+02	3.36+02	9.23+03	1.84+03	2.16+02	2.53+02	7.60+07	1.26+06	9.13+08
400	16	6.84+02	3.36+02	9.26+03	1.85+03	2.17+02	2.53+02	7.62+07	1.26+06	9.15+08
400	17	7.18+02	3.37+02	9.56+03	1.91+03	2.20+02	2.58+02	7.87+07	1.28+06	9.31+08
400	18	1.05+01	3.48+02	1.26+02	2.51+03	2.54+02	3.04+02	1.04+06	1.48+06	1.16+07
400	19	3.85+01	4.58+02	4.33+02	8.64+03	6.73+02	1.04+01	3.56+06	3.93+06	3.77+07
400	20	1.33+01	1.64+01	3.60+01	7.19+02	7.45+01	1.75+00	2.96+05	4.34+05	6.32+06
400	21	1.87+00	1.23+00	3.26+00	6.50+01	9.04+00	2.23+01	2.68+04	5.27+04	6.44+05
400	22	1.96+00	9.09+00	2.56+01	5.12+00	8.10+01	2.01+02	2.11+03	4.72+03	7.26+04
400	23	1.96+00	3.69+01	1.05+02	2.10+01	3.40+02	8.50+02	8.66+03	1.98+02	3.07+03
400	24	1.97+00	5.39+01	1.54+02	3.08+01	5.00+02	1.25+03	1.27+02	2.91+02	4.52+03

TABLE 24

## MOLYBDENUM XXXII

INTENSITY RATIO  $I(^nL \rightarrow ^{n'}L') / I(^3P \rightarrow ^3S)$ 

T(KEV)	L <sub>NG</sub>	N	3D-3P	4S-3P	4P-3S	4P-3D	4F-3P	4F-3D	4P-4S	4F-4P	4F-4D
500	15	7.15-02	4.72-02	1.41-02	2.61-03	3.21-02	3.72-02	1.16-06	1.87-06	1.34-07	
500	16	7.18-02	4.72-02	1.41-02	2.82-03	3.21-02	3.73-02	1.16-06	1.87-06	1.75-07	
500	17	7.51-02	4.74-02	1.45-02	2.90-03	3.26-02	3.79-02	1.16-06	1.91-06	1.37-07	
500	18	1.07-01	4.88-02	1.85-02	3.69-03	3.73-02	4.42-02	1.52-06	2.17-06	1.61-07	
500	19	3.81-01	6.31-02	5.90-02	1.18-02	9.40-02	1.43-01	4.85-06	5.48-06	5.16-07	
500	20	1.36-03	2.17-01	4.78-01	9.53-02	1.00-00	2.36-00	3.93-05	5.83-05	8.45-06	
500	21	1.96-00	1.61-00	4.34-00	8.66-01	1.22-01	3.16-01	3.57-04	7.11-04	1.10-04	
500	22	2.05-00	1.21-01	3.46-01	6.91-00	1.11-02	2.80-02	2.65-03	6.49-03	1.11-03	
500	23	2.06-00	5.12-01	1.49-02	2.97-01	4.90-02	1.24-03	1.22-02	2.86-02	4.42-03	
500	24	2.07-00	7.71-01	2.24-02	4.48-01	7.41-02	1.88-03	1.84-02	4.32-02	6.78-03	
600	15	7.39-02	5.91-02	1.88-02	3.76-03	4.17-02	4.80-02	1.55-06	2.43-06	1.73-07	
600	16	7.42-02	5.90-02	1.89-02	3.77-03	4.17-02	4.81-02	1.55-06	2.43-06	1.74-07	
600	17	7.74-02	5.92-02	1.93-02	3.86-03	4.23-02	4.88-02	1.59-06	2.47-06	1.76-07	
600	18	1.09-01	6.08-02	2.41-02	4.80-03	4.81-02	5.65-02	1.98-06	2.81-06	2.04-07	
600	19	3.76-01	7.77-02	7.19-02	1.44-02	1.17-01	1.74-01	5.92-06	6.81-06	6.29-07	
600	20	1.34-00	2.59-01	5.69-01	1.14-01	1.20-00	2.84-00	4.68-05	7.01-05	1.13-05	
600	21	2.02-00	1.91-00	5.19-00	1.03-00	1.47-01	3.74-01	4.27-04	8.58-04	1.35-04	
600	22	2.12-00	1.44-01	4.18-01	8.35-00	1.36-02	3.45-02	3.44-03	7.93-03	1.25-03	
600	23	2.13-00	6.34-01	1.86-02	3.71-01	6.21-02	1.58-03	1.53-02	3.62-02	5.72-03	
600	24	2.13-00	9.78-01	2.88-02	5.74-01	6.63-02	2.46-03	2.37-02	5.61-02	8.67-03	

TABLE 25

**MOLYBDENUM XXXII**

 INTENSITY RATIO  $I(\text{II L} \rightarrow \text{I'L}')/I(\text{3P} \rightarrow \text{3S})$ 

T(KEV)	LOG N	3D-3P	4S-3P	4P-3S	4P-3D	4D-3P	4F-3P	4P-4S	4F-4P	4F-4D
800	15	7.72-02	7.75-02	2.74-02	5.47-03	5.80-02	6.56-02	2.26-06	3.38-06	2.37-07
800	16	7.75-02	7.75-02	2.75-02	5.48-03	5.80-02	6.56-02	2.26-06	3.38-06	2.37-07
800	17	8.05-02	7.77-02	2.80-02	5.60-03	5.88-02	6.65-02	2.31-06	3.43-06	2.46-07
800	18	1.10-01	7.97-02	3.37-02	6.73-03	6.62-02	7.61-02	2.77-06	3.88-06	2.75-07
800	19	3.04-01	9.99-02	9.12-02	1.82-02	1.52-01	2.19-01	7.51-06	8.84-06	7.89-07
800	20	1.38-00	3.17-01	6.91-01	1.38-01	1.47-00	3.48-00	5.69-05	6.59-05	1.26-05
800	21	2.09-00	2.32-00	6.34-00	1.26-00	1.81-01	4.69-01	5.22-04	1.66-03	1.69-04
800	22	2.21-00	1.77-01	5.19-01	1.04-01	1.71-02	4.40-02	4.27-03	9.99-03	1.59-03
800	23	2.22-00	8.18-01	2.44-02	4.86-01	8.26-02	2.13-03	2.01-02	4.92-02	7.69-03
800	24	2.22-00	1.31-02	3.92-02	7.82-01	1.33-03	3.43-03	3.22-02	7.77-02	1.24-02
1000	15	7.94-12	9.10-02	3.47-02	6.92-03	7.07-02	7.87-02	2.85-06	4.12-06	2.84-07
1000	16	7.96-12	9.10-02	3.47-02	6.93-03	7.08-02	7.88-02	2.86-06	4.13-06	2.85-07
1000	17	8.24-12	9.12-02	3.54-02	7.06-03	7.16-02	7.98-02	2.91-06	4.18-06	2.88-07
1000	18	1.10-01	9.34-02	4.15-02	8.20-03	8.00-02	9.05-02	3.42-06	4.67-06	3.27-07
1000	19	3.52-01	1.15-01	1.04-01	2.08-02	1.76-01	2.46-01	8.58-06	1.03-05	8.89-07
1000	20	1.37-00	3.53-01	7.61-01	1.52-01	1.63-00	3.84-00	6.26-05	9.51-05	1.39-05
1000	21	2.13-00	2.56-00	7.01-00	1.40-00	2.01-01	5.28-01	5.77-04	1.17-03	1.91-04
1000	22	2.26-00	1.96-01	5.81-01	1.16-01	1.93-02	5.00-02	4.78-03	1.13-02	1.81-03
1000	23	2.28-00	9.45-01	2.84-02	5.66-01	9.70-02	2.52-03	2.33-02	5.66-02	9.10-03
1000	24	2.28-00	1.56-02	4.71-02	9.40-01	1.62-03	4.19-03	3.88-02	9.42-02	1.51-02

TABLE 26

## MOLYBDENUM XXXII

INTENSITY RATIO  $I(\text{M L} - \text{M'L})/I(3\text{P} - 3\text{S})$ 

T(EV)	L6G	H	3D-3P	4S-3P	4P-3S	4P-3D	4D-3P	4F-3S	4F-3D	4F-4S	4G-4P	4F-4P
1500	15		8.25+02	1.12+01	4.80+02	9.58+03	9.24+02	1.0.60+02	3.95+06	5.30+07	3.01+07	
1500	16		6.27+02	1.12+01	4.81+02	9.60+03	9.25+02	1.0.60+01	3.96+06	5.39+06	3.01+07	
1500	17		6.52+02	1.12+01	4.87+02	9.73+03	9.34+02	1.0.61+01	4.01+06	5.45+06	3.05+07	
1500	18		1.09+01	1.15+01	5.53+02	1.0.62+01	1.0.63+01	1.0.63+01	4.05+06	6.01+06	4.06+07	
1500	19		5.27+01	1.38+01	1.22+01	2.40+02	2.11+01	2.79+01	1.0.61+05	1.23+05	1.0.61+05	
1500	20		1.33+00	3.93+01	8.26+01	1.65+01	1.79+00	4.13+00	6.80+05	1.0.64+04	1.49+05	
1500	21		2.18+00	2.79+00	7.66+00	1.53+00	2.21+01	5.90+01	6.30+04	1.0.29+03	2.13+04	
1500	22		2.34+00	2.17+01	6.48+01	1.20+01	2.17+02	5.70+02	5.33+03	1.0.27+02	2.0.6+03	
1500	23		2.36+00	1.12+02	3.39+02	6.77+01	1.17+03	3.07+03	2.79+02	6.25+02	1.11+02	
1500	24		2.36+00	1.97+02	5.90+02	1.20+02	2.08+03	5.44+03	4.93+02	1.21+01	1.97+02	
2000	15		8.41+02	1.24+01	5.69+02	1.13+02	1.06+01	1.12+01	4.68+06	6.16+06	4.06+07	
2000	16		6.43+02	1.24+01	5.69+02	1.14+02	1.06+01	1.12+01	4.68+06	6.17+06	4.06+07	
2000	17		6.65+02	1.24+01	5.76+02	1.15+02	1.07+01	1.13+01	4.74+06	6.23+06	4.10+07	
2000	18		1.08+01	1.27+01	6.41+02	1.28+02	1.17+01	1.25+01	5.28+06	6.81+06	4.53+07	
2000	19		3.07+01	1.50+01	1.30+01	2.60+02	2.27+01	2.88+01	1.07+05	1.32+05	1.04+06	
2000	20		1.24+00	4.04+01	8.30+01	1.66+01	1.80+00	4.08+00	6.83+05	1.05+04	1.47+05	
2000	21		2.26+00	2.82+00	7.72+00	1.54+00	2.23+01	6.01+01	6.35+04	1.30+03	2.17+04	
2000	22		2.38+00	2.21+01	6.61+01	1.32+01	2.23+02	5.88+02	5.44+03	1.30+02	2.12+03	
2000	23		2.39+00	1.19+02	3.63+02	7.25+01	1.27+03	3.32+03	2.99+02	7.38+02	1.20+02	
2000	24		2.40+00	2.20+02	6.73+02	1.34+02	2.35+03	6.18+03	5.54+02	1.37+01	2.23+02	